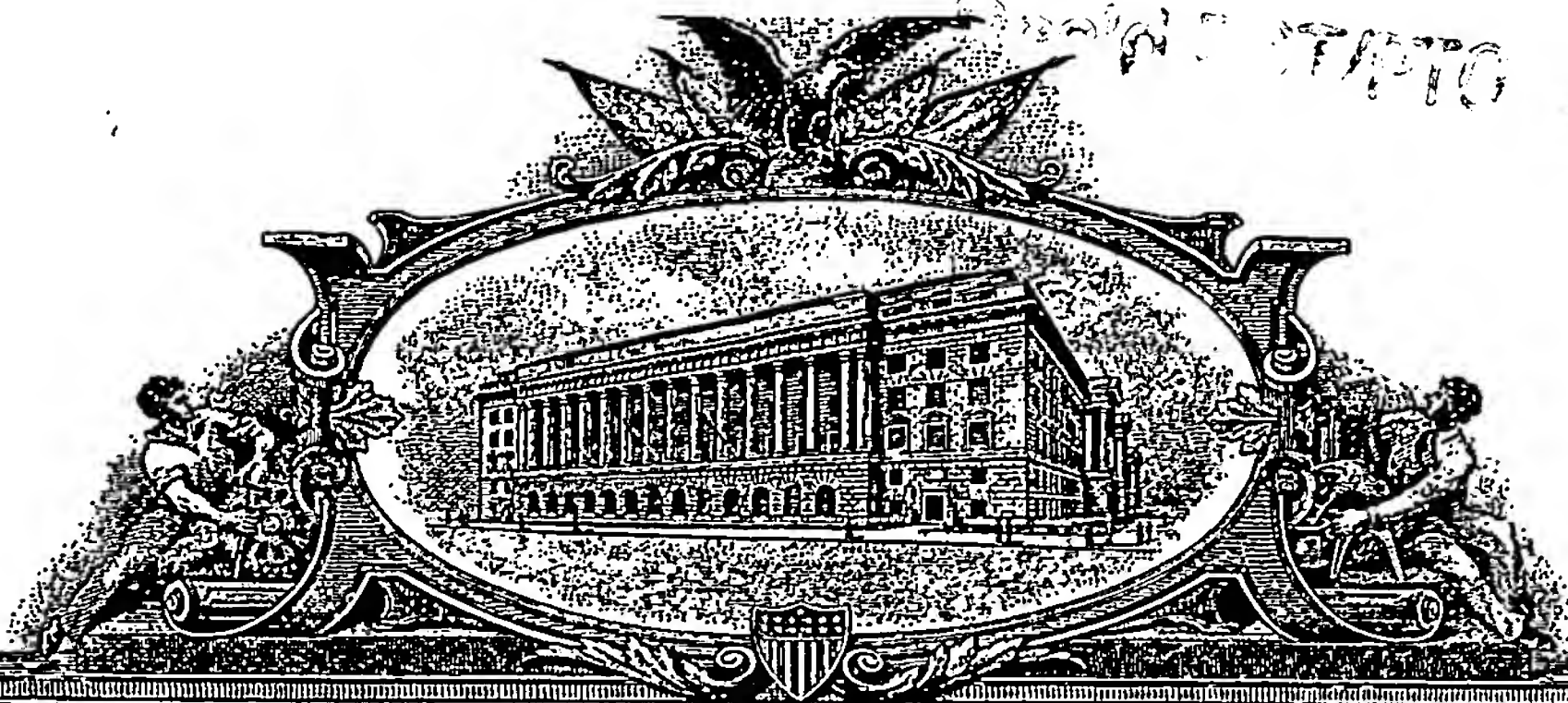


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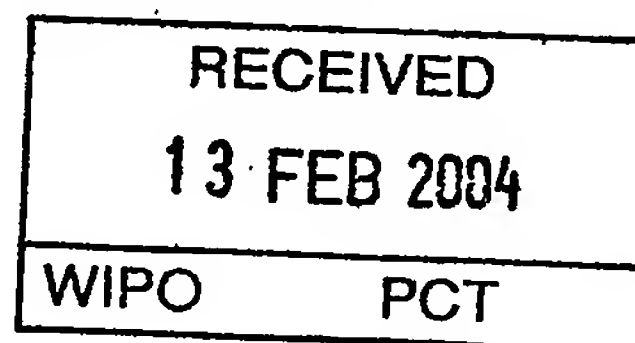
February 09, 2004

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APPLICATION THAT MET THE REQUIREMENTS TO BE GRANTED A
FILING DATE.**

APPLICATION NUMBER: 10/390,487

FILING DATE: March 17, 2003

RELATED PCT APPLICATION NUMBER: PCT/US03/36256



**By Authority of the
COMMISSIONER OF PATENTS AND TRADEMARKS**



R. Blakeney
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Certifying Officer

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UTILITY PATENT APPLICATION TRANSMITTAL
(Larg Entity)*(Only for new nonprovisional applications under 37 CFR 1.53(b))*Docket No.
88932Total Pages in this Submission
60**TO THE ASSISTANT COMMISSIONER FOR PATENTS**Box Patent Application
Washington, D.C. 20231

Transmitted herewith for filing under 35 U.S.C. 111(a) and 37 C.F.R. 1.53(b) is a new utility patent application for an invention entitled:

FOLDED DIPOLE ANENNA, COAXIAL TO MICROSTRIP TRANSITION, AND RETAINING ELEMENT

and invented by:

Bisiules et al.

If a CONTINUATION APPLICATION, check appropriate box and supply the requisite information:

☐ Continuation ☐ Divisional ☐ Continuation-in-part (CIP) of prior application No.: _____

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Enclosed are:

Application Elements

1. ☒ Filing fee as calculated and transmitted as described below
2. ☒ Specification having 26 pages and including the following:
 - a. ☒ Descriptive Title of the Invention
 - b. ☐ Cross References to Related Applications (if applicable)
 - c. ☐ Statement Regarding Federally-sponsored Research/Development (if applicable)
 - d. ☐ Reference to Sequence Listing, a Table, or a Computer Program Listing Appendix
 - e. ☒ Background of the Invention
 - f. ☒ Brief Summary of the Invention
 - g. ☒ Brief Description of the Drawings (if filed)
 - h. ☒ Detailed Description
 - i. ☒ Claim(s) as Classified Below
 - j. ☒ Abstract of the Disclosure

UTILITY PATENT APPLICATION TRANSMITTAL (Large Entity)

(Only for new nonprovisional applications under 37 CFR 1.53(b))

Docket No.
88932

Total Pages in this Submission
60

Application Elements (Continued)

3. ☒ Drawing(s) (when necessary as prescribed by 35 USC 113)
- a. ☒ Formal Number of Sheets 20
- b. ☐ Informal Number of Sheets
4. ☒ Oath or Declaration
- a. ☐ Newly executed (original or copy) ☒ Unexecuted
- b. ☐ Copy from a prior application (37 CFR 1.63(d)) (for continuation/divisional application only)
- c. ☒ With Power of Attorney ☐ Without Power of Attorney
- d. ☐ DELETION OF INVENTOR(S)
Signed statement attached deleting inventor(s) named in the prior application,
see 37 C.F.R. 1.63(d)(2) and 1.33(b).
5. ☐ Incorporation By Reference (usable if Box 4b is checked)
The entire disclosure of the prior application, from which a copy of the oath or declaration is supplied under Box 4b, is considered as being part of the disclosure of the accompanying application and is hereby incorporated by reference therein.
6. ☐ CD ROM or CD-R in duplicate, large table or Computer Program (Appendix)
7. ☒ Application Data Sheet (See 37 CFR 1.76)
8. ☐ Nucleotide and/or Amino Acid Sequence Submission (if applicable, all must be included)
- a. ☐ Computer Readable Form (CRF)
- b. ☐ Specification Sequence Listing on:
- i. ☐ CD-ROM or CD-R (2 copies); or
- ii. ☐ Paper
- c. ☐ Statement(s) Verifying Identical Paper and Computer Readable Copy

Accompanying Application Parts

9. ☐ Assignment Papers (cover sheet & document(s))
10. ☐ 37 CFR 3.73(B) Statement (when there is an assignee)
11. ☐ English Translation Document (if applicable)
12. ☐ Information Disclosure Statement/PTO-1449 ☐ Copies of IDS Citations
13. ☐ Preliminary Amendment
14. ☒ Return Receipt Postcard (MPEP 503) (Should be specifically itemized)
15. ☐ Certified Copy of Priority Document(s) (if foreign priority is claimed)
16. ☒ Certificate of Mailing
- ☐ First Class ☒ Express Mail (Specify Label No.): EL867963572US

UTILITY PATENT APPLICATION TRANSMITTAL (Large Entity)

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Docket No.
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Total Pages in this Submission
60

Accompanying Application Parts (Continued)

17. ☒ Additional Enclosures (please identify below):

I hereby certify that this paper is being deposited with the United States Postal Service as Express Mail in an envelope addressed to: Commissioner for Patents, Washington, D.C. 20231, on

Date: 3/17/03 [Signature]
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Request That Application Not Be Published Pursuant To 35 U.S.C. 122(b)(2)

18. ☐ Pursuant to 35 U.S.C. 122(b)(2), Applicant hereby requests that this patent application not be published pursuant to 35 U.S.C. 122(b)(1). Applicant hereby certifies that the invention disclosed in this application has not and will not be the subject of an application filed in another country, or under a multilateral international agreement, that requires publication of applications 18 months after filing of the application.

Warning

An applicant who makes a request not to publish, but who subsequently files in a foreign country or under a multilateral international agreement specified in 35 U.S.C. 122(b)(2)(B)(i), must notify the Director of such filing not later than 45 days after the date of the filing of such foreign or international application. A failure of the applicant to provide such notice within the prescribed period shall result in the application being regarded as abandoned, unless it is shown to the satisfaction of the Director that the delay in submitting the notice was unintentional.

UTILITY PATENT APPLICATION TRANSMITTAL (Large Entity)

(Only for new nonprovisional applications under 37 CFR 1.53(b))

Docket No.
88932

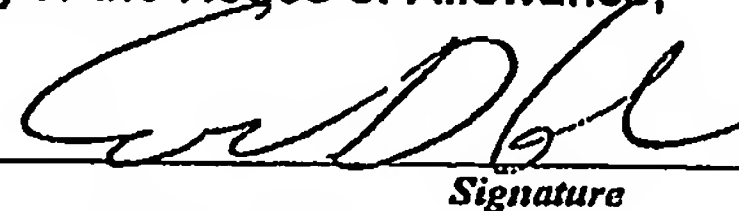
Total Pages in this Submission
60

Fee Calculation and Transmittal

CLAIMS AS FILED

For	#Filed	#Allowed	#Extra	Rate	Fee
Total Claims	41	- 20 =	21	x \$18.00	\$378.00
Indep. Claims	9	- 3 =	6	x \$84.00	\$504.00
Multiple Dependent Claims (check if applicable) <input type="checkbox"/>					\$0.00
BASIC FEE					\$750.00
OTHER FEE (specify purpose) _____					\$0.00
TOTAL FILING FEE					\$1,632.00

- ☒ A check in the amount of \$1,632.00 to cover the filing fee is enclosed.
- ☒ The Commissioner is hereby authorized to charge and credit Deposit Account No. 23-0920 as described below. A duplicate copy of this sheet is enclosed.
- ☐ Charge the amount of _____ as filing fee.
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- ☐ Charge the issue fee set in 37 C.F.R. 1.18 at the mailing of the Notice of Allowance, pursuant to 37 C.F.R. 1.311(b).



Signature

Eric D. Cohen, Esq.
Reg. No. 38,110

Dated: March 17, 2003

cc:

APPLICATION DATA SHEET**APPLICATION INFORMATION**

Application number::	Not Yet Assigned
Filing Date::	March 17, 2003
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Attorney Docket Number::	88932
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Suggested Drawing Figure::	1
Total Drawing Sheets::	20
Formal Drawings::	Yes
Small Entity?::	No
Benefit of Priority Claimed From::	N/A

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 Registration Number Three: 28,903
 Registration Number Four: 27,429
 Registration Number Five: 25,060
 Registration Number Six: 22,053
 Registration Number Seven: 27,466

Registration Number Eight:	29,434
Registration Number Nine:	29,054
Registration Number Ten:	29,381
Registration Number Eleven:	34,044
Registration Number Twelve:	27,600
Registration Number Thirteen:	34,137
Registration Number Fourteen:	38,110
Registration Number Fifteen:	39,724
Registration Number Sixteen:	39,021
Registration Number Seventeen:	37,963
Registration Number Eighteen:	37,135
Registration Number Nineteen:	40,604
Registration Number Twenty:	37,435

ASSIGNMENT INFORMATION

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Assignee Address Line Two::	
Assignee City::	
Assignee State::	
Assignee Postal Code::	
Assignee Country::	

FOLDED DIPOLE ANTENNA, COAXIAL TO MICROSTRIP TRANSITION, AND RETAINING ELEMENT

FIELD OF THE INVENTION

5

A first aspect of the present invention relates generally to folded dipole antennas.

A second aspect of the present invention relates to a coaxial to microstrip transition. A third aspect of the present invention relates to a retaining element.

All aspects of the invention are typically but not exclusively for use in wireless
10 mobile communications systems

BACKGROUND OF THE INVENTION

US6317099 and US6285666 describe a folded dipole antenna with a ground
15 plane; and a conductor having a microstrip feed section extending adjacent the
ground plane and spaced therefrom by a dielectric, a radiator input section, and at
least one radiating section integrally formed with the radiator input section and the
feed section. The radiating section includes first and second ends, a fed dipole and
a passive dipole, the fed dipole being connected to the radiator input section, the
20 passive dipole being disposed in spaced relation to the fed dipole to form a gap, the
passive dipole being shorted to the fed dipole at the first and second ends.

The radiating section is driven with a feed which is not completely balanced. An
unbalanced feed can lead to unbalanced currents on the dipole arms which can
25 cause beam skew in the plane of polarization (vertical pattern for a v-pol antenna,
horizontal pattern for a h-pol antenna, vertical and horizontal patterns for a slant pol
antenna), increased cross-polar isolation in the far field and increased coupling
between polarizations for a dual polarized antenna.

A stripline folded dipole antenna is described in US5917456. A disadvantage of a stripline arrangement is that a pair of ground planes is required, resulting in additional expense and bulk.

- 5 US4837529 describes a microstrip to coaxial side-launch transition. A microstrip transmission line is provided on a first side of a ground plane, and a coaxial transmission line is provided on a second side of the ground plane opposite to the first side of the ground plane. The coaxial transmission line has a central conductor directly soldered to the microstrip line. Direct soldering to the microstrip line has a
- 10 number of disadvantages. Firstly, the integrity of the joint cannot be guaranteed. Secondly, it is necessary to construct the microstrip line from a metal which allows the solder to flow. The coaxial cylindrical conductor sleeve is also directly soldered to the ground plane. Direct soldering to the ground plane has the disadvantages given above, and also the further disadvantage that the ground plane will act as a
- 15 large heat sink, requiring a large amount of heat to be applied during soldering.

BRIEF DESCRIPTION OF EXEMPLARY EMBODIMENT

20 An exemplary embodiment provides in a first aspect a dual polarized folded dipole antenna comprising:

a first unit configured for transmitting and/or receiving signals in a first polarization direction; and

a second unit configured for transmitting and/or receiving signals in a second polarization direction different to the first polarization direction,

25 wherein each unit includes a conductor having a feed section, a radiator input section, and at least one radiating section integrally formed with the radiator input section and the feed section, the radiating section including first and second ends, a fed dipole and a passive dipole, the fed dipole being connected to the radiator input section, the passive dipole being disposed in spaced relation to the fed dipole

to form a gap, the passive dipole being shorted to the fed dipole at the first and second ends.

The exemplary embodiment provides in a second aspect a folded dipole antenna
5 comprising:

a ground plane

a conductor having a feed section extending adjacent the ground plane and
spaced therefrom by a dielectric, a radiator input section, and at least one radiating
section integrally formed with the radiator input section and the feed section, the
10 radiating section including first and second ends, a fed dipole and a passive dipole,
the fed dipole being connected to the radiator input section, the passive dipole
being disposed in spaced relation to the fed dipole to form a gap, the passive dipole
being shorted to the fed dipole at the first and second ends,

wherein the feed section is a microstrip feed section having an adjacent ground
15 plane on one side only, and

wherein the radiator input section includes a balun transformer.

The balun transformer provides a balanced feed and obviates the problems
discussed above.

20

The exemplary embodiment provides in a third aspect a folded dipole antenna
comprising:

a ground plane

a conductor having a feed section extending adjacent the ground plane and
25 spaced therefrom by a dielectric, a radiator input section, and at least one radiating
section integrally formed with the radiator input section and the feed section, the
radiating section including first and second ends, a fed dipole and a passive dipole,
the fed dipole being connected to the radiator input section, the passive dipole
being disposed in spaced relation to the fed dipole to form a gap, the passive dipole
30 being shorted to the fed dipole at the first and second ends,

wherein the feed section is a microstrip feed section having an adjacent ground plane on one side only, and

wherein the radiator input section includes a splitter, first and second feedlines which meet said feed section at said splitter so as to complete a closed loop
5 including the first and second feedlines and the radiating section, and a phase delay element for introducing a phase difference between the first and second feedlines.

The exemplary embodiment provides in a fourth aspect a coaxial to microstrip transition comprising:

10 a ground plane;

a microstrip transmission line on a first side of the ground plane;

a coaxial transmission line on a second side of the ground plane opposite to the first side of the ground plane, the coaxial transmission line having a central conductor coupled to the microstrip line, a coaxial cylindrical conductor sleeve
15 coupled to the ground plane, and a dielectric material between the central conductor and the sleeve,

a conductive ground transition body in conductive engagement with the sleeve;
and

a ground locking member applying a force to the ground transition body so as to
20 force the ground transition body into conductive engagement with the ground plane.

This construction obviates the need for a direct solder joint between the sleeve and the ground plane.

25

The exemplary embodiment provides in a fifth aspect a coaxial to microstrip transition comprising:

a ground plane;

a microstrip transmission line on a first side of the ground plane;

a coaxial transmission line on a second side of the ground plane opposite to the first side of the ground plane, the coaxial transmission line having a central conductor coupled to the microstrip line, a coaxial cylindrical conductor sleeve coupled to the ground plane, and a dielectric material between the central
5 conductor and the sleeve,

a conductive line transition body in conductive engagement with the central conductor; and

a line locking member applying a force to the line transition body so as to force the line transition body into conductive engagement with the microstrip line.
10

This construction obviates the need for a direct solder joint between the central conductor and the microstrip line.

15

The exemplary embodiment provides in a sixth aspect a method of constructing a coaxial to microstrip transition, the method comprising:

arranging a microstrip transmission line on a first side of a ground plane;
arranging a coaxial transmission line on a second side of the ground plane
20 opposite to the first side of the ground plane, the coaxial transmission line having a central conductor coupled to the microstrip line, a coaxial cylindrical conductor sleeve coupled to the ground plane, and a dielectric material between the central conductor and the sleeve,

arranging a conductive ground transition body in conductive engagement with
25 the sleeve; and

applying a force to the ground transition body so as to force the ground transition body into conductive engagement with the ground plane.

The exemplary embodiment provides in a seventh aspect a method of
30 constructing a coaxial to microstrip transition, the method comprising:

arranging a microstrip transmission line on a first side of a ground plane;
arranging a coaxial transmission line on a second side of the ground plane
opposite to the first side of the ground plane, the coaxial transmission line having a
central conductor coupled to the microstrip line, a coaxial cylindrical conductor
5 sleeve coupled to the ground plane, and a dielectric material between the central
conductor and the sleeve,
arranging a conductive line transition body in conductive engagement with the
central conductor; and
applying a force to the line transition body so as to force the line transition body
10 into conductive engagement with the microstrip line.

The exemplary embodiment provides in an eighth aspect an electrically
insulating retaining element for retaining together adjacent ends of a pair of dipoles,
the element comprising a body portion having a pair of sockets on opposite side of
15 the body portion; and a pair of resilient members which each obstruct a respective
socket and resiliently flex, when in use, to admit an end of a dipole into the socket.

The exemplary embodiment provides in a ninth aspect a dipole assembly
comprising two or more dipoles having adjacent ends retained together by
20 electrically insulating retaining elements, each element comprising a body portion
having a pair of sockets on opposite side of the body portion; and a pair of resilient
members which each obstruct a respective socket and resiliently flex, when in use,
to admit an end of a dipole into the socket.

25 BRIEF DESCRIPTION OF THE DRAWINGS

Illustrative embodiments of the invention will now be described with reference to
the accompanying drawings to disclose the advantageous teachings of the present
invention.

- Figure 1 is an isometric view of a dual polarization folded dipole antenna according to one embodiment of the present invention;
- Figure 2 is a side view of the dual polarization folded dipole antenna of Figure 1;
- Figure 3 is an isometric view of the $+45^\circ$ antenna unit;
- 5 Figure 3A is a cross-sectional view through a DC ground connection;
- Figure 4 is an isometric view of the -45° antenna unit;
- Figure 5 is an isometric view of a single radiating module of the antenna of Figure 1;
- Figure 6A is an isometric view showing the method of fixing the antenna units to
- 10 the ground plane, in the antenna of Figure 1;
- Figure 6B is an isometric view of the dielectric spacer shown in Figure 6A;
- Figure 6C is a side view of the assembled ground plane, dielectric spacer and antenna unit;
- Figure 7A is an isometric top view of the dielectric clip;
- 15 Figure 7B is an isometric bottom view of the dielectric clip;
- Figure 7C is an isometric view of two adjacent radiating sections;
- Figure 7D is an isometric view of the radiating sections with a clip inserted;
- Figure 8 is an isometric view of a dual polarization folded dipole antenna having a single radiating module, according to a second embodiment of the present
- 20 invention;
- Figure 9 is a side view of the coaxial to microstrip transition;
- Figure 10 is a cross-sectional view of the coaxial to microstrip transition of Figure 9;
- Figure 11 is an exploded view of the coaxial to microstrip transition of Figure 9;
- 25 Figure 12 is a first perspective view of the coaxial to microstrip transition of Figure 9;
- Figure 13 is a second perspective view of the coaxial to microstrip transition of Figure 9;
- Figure 14 is a plan view of an alternative radiating section configuration. And
- 30 Figure 15 is a schematic side view of a pair of base stations.

DESCRIPTION OF ILLUSTRATIVE EMBODIMENTS

Figures 1 and 2 show a slant polarized dual polarization folded dipole antenna 100 according to the invention. A reflector tray is formed by a ground plane 101, lower and upper end walls 103, 104 and side walls 102. A $+45^\circ$ integrally formed microstrip antenna unit 300 (shown in Figure 3) and a -45° integrally formed microstrip antenna unit 400 (shown in Figure 4) are mounted adjacent, and substantially parallel to, the ground plane 101, as described in detail below.

Together, the radiating sections of the microstrip antenna units 300, 400 form a number of generally circular radiating modules 500 which are spaced apart along an antenna axis. The antenna is generally mounted in use on a base station mast with the antenna axis oriented in a vertical direction. The $+45^\circ$ antenna unit 300 radiates with a polarization at $+45^\circ$ to the antenna axis, while the -45° antenna unit 400 radiates with a polarization at -45° to the antenna axis.

Figure 3 shows the $+45^\circ$ microstrip antenna unit 300. The antenna unit comprises a feed section 320, radiator input sections (including dipole feed legs 324 and 325, and phase delay lines 322, 323) and radiating sections 301 and 302.

The feed section, radiator input sections and radiating sections are formed integrally, by cutting or stamping from a flat sheet of conductive material such as, for example, a metal sheet comprised of aluminum, copper, brass or alloys thereof. Since the antenna unit is formed integrally, the number of mechanical contacts necessary is reduced, improving the intermodulation distortion (IMD) performance of the antenna 100. The feed section 320 branches out from a single RF input section 340 (partially obscured) that is electrically connected to a coaxial transmission line (not shown in Figures 1-4) via a transition shown in detail in Figures 9-13 and described in further detail below. The coaxial transmission line passes along the rear side of the ground plane 101, through one of the slots 110 or 111 in the ground plane (shown in Figure 1) and through one of the holes 120 or

- 121 in the lower end wall 103. Many other paths for the transmission line may also be suitable. The transmission line is generally electrically connected to an RF device such as a transmitter or a receiver. In one embodiment, the RF input section 340 directly connects to the RF device. The feed section 320 also includes a DC ground connection, positioned at the end of a quarter wavelength stub 342. The DC ground connection is shown in cross-section in Figure 3A. The stub 342 has a circular pad 341 at its end with a hole 344. A bolt 343 passes through the hole 344 and a hole 345 in the ground plane 101. A cylindrical metal spacer 346 has an external diameter greater than the internal diameters of the holes 344, 345 and engages the pad 341 at one end and the ground plane 101 at the other end. The bolt 343 is threaded at its distal end and an internally threaded nut 346 compresses the pad 341 and the groundplane 101 together with a given torque to ensure a tight metal joint for good intermodulation performance.
- 15 The feed section 320 further includes a number of meandering phase delay lines 321, to provide a desired phase relationship between the radiating sections 301, 302 and between the modules 500. In the embodiment shown in Figure 3, the meandering phase delay lines 321 are configured so that the all radiating sections 301, 302 and all modules 500 are at the same phase. Alternatively the lines 321 may be configured to give a fixed phase difference (and hence downtilt) between the modules.

Figure 4 shows the -45° microstrip antenna unit 400. The unit is similar to the $+45^\circ$ antenna unit, and similar elements are given the same reference numerals, increased by 100. For instance the equivalent to the $+45^\circ$ radiating sections 301, 302 are -45° radiating sections 401, 402. It will be seen by a comparison of Figures 3 and 4 that the $+45^\circ$ unit 300 and -45° unit 400 interlock together to form the dual-polarized modules 500.

Figure 5 shows an exemplary one of the radiating modules 500. The radiating module comprises radiating sections 301, 302, 401 and 402 arranged in a circular "box" configuration around a central region. An alternative "square" box configuration is shown in Figure 14. The radiating sections are similar in construction and only radiating section 302 will be described in full. Radiating section 302 includes a fed dipole (comprising a first quarter-wavelength monopole 304 and a second quarter-wavelength monopole 305) and a passive dipole 306, separated by a gap 331. End sections of the conductor (concealed in Figure 5 beneath a clip 700) at opposing ends of the gap 331 electrically short the monopoles 304,305 with the passive dipole 306. The first quarter-wavelength monopole 304 is connected to the first dipole feed leg 324 at bend 330. The first dipole feed leg 324 is connected to the feed section 320 at a splitter junction 326. The second quarter-wavelength monopole 305 is connected to the second dipole feed leg 325 at bend 329. The second dipole feed leg 325 is connected to a 180° phase delay line 322 at bend 327. The phase delay line 322 is connected at its other end to the splitter junction 326. The length of the phase delay line 322 is selected such that the dipole feed legs 324 and 325 have a phase difference of 180°, thus providing a balanced feed to the fed dipole. It will be appreciated that the feed legs 324,325, radiating section and phase delay line 322 together define a closed loop. The phased line 322 and splitter junction 326 together act as a balun (a balanced to unbalanced transformer).

In a first alternative arrangement (not shown), the shorter feed path (that is, the feed path between the splitter junction 326 and the feed leg 324) may include two quarter-wave separated open half-wavelength stubs, as described in US6515628. The stubs compensate or balance the phase across the frequency band of interest.

In a second alternative arrangement (not shown), the balun formed by the splitter junction 326 and phase delay line 322 may be replaced by a Schiffman coupler as described in US5917456.

Together the dipole feed legs have an intrinsic impedance that is adjusted to match the radiating section 302 to the feed section. This impedance is adjusted, in part, by varying the width of the dipole feed legs 324, 325 and the gap 332. The bends
5 are such that the dipole feed legs 324 and 325 are substantially perpendicular to the feed section 320 and the ground plane 101, and the radiating section 302 is substantially parallel to the feed section 320 and the ground plane 101. The radiating sections 301, 302, 401 and 402 are mechanically connected by dielectric clip 700, which is further described below. This connection provides greater
10 stability and strength, and ensures correct spacing of the radiating sections.

The microstrip antenna units 300 and 400 could be spaced from the ground plane 101 by any dielectric, such as air, foam, etc. In the preferred embodiment, the microstrip antenna units are spaced from the ground plane by air, and are fixed to
15 the ground plane using dielectric spacers 600 shown in Figure 6A and in detail in Figure 6B, although other types of dielectric support could also be used. Other possible dielectric supports include nuts and bolts with dielectric washers, screws with dielectric washers, etc.

20 The dielectric spacers 600 have a body portion 640, stub 630, and lugs 610 and 620 which fit into a slot 601 and a hole 602 respectively in the ground plane. The lug 610 comprises a neck 611 and a lower transverse elongate section 612. The lug 620 comprises two legs having a lower sloping section 621, a shoulder 622 and neck 623. The legs are resilient so that they bend inwardly when forced
25 through the hole 602 in the ground plane, and spring back when the shoulder 622 has passed through. To fix the dielectric spacer 600 to the ground plane 101 the elongate section 612 is passed through the slot 601; the dielectric spacer is rotated through 90 degrees, such that the elongate section cannot pass back through the slot 601; and the lug 620 is forced through the hole 602. The shoulders 622 and
30 elongate section 612 are spaced from the body portion 640 by a distance

corresponding to the thickness of the ground plane so that the dielectric spacer and ground plane are fixed together when the shoulders and elongated section engage the back side of the ground plane. The stub 630 is received in a hole 603 in the feed section 320 or 420. The top of the stub 630 is then deformed by heating
5 such that the feed section 320 or 420, body portion 640 and ground plane 101 are fixed together, as shown in the cross-section of Figure 6C. Figure 6C also shows the air gap 650 between the air suspended microstrip feed section 320 and the ground plane 101. The spacer 600 is precisely machined so as to maintain a desired gap.

10

The dielectric clip 700 is shown in more detail in Figures 7A and 7B. The clip comprises a body portion formed with a longitudinal rib 707, and a pair of sockets 701,702 which receive the ends of the radiating sections 301,402. Slots 703,704 are provided in the base of the sockets 701,702. A pair of spring arms 705,706
15 extend transversely from the rib 707. The spring arms 705,706 are identical and are each formed with a catch at their distal end including an angled ramp 710 and locking face 711.

The clip is formed using a two-part mold, and the purpose of slots 703,704 is to
20 enable the under-surface of spring arms 705,706 to be properly molded.

Figure 7C shows the ends of radiating sections 301,402 before the clip 700 is attached. The fed monopoles 304,305 are shorted to the passive dipole 306 by end sections 307. The end section 307 has an inner edge 309 and inner face 308.
25 The clip 700 is mounted by pulling the radiating section 402 away to give sufficient clearance, and sliding the clip into place with the end section 307 received in the socket 701 as shown in Figure 7D. As the clip slides into place, the ramp 710 (which partially obstructs the socket) engages the end section 307, causing the spring arm 705 to resiliently flex upwardly until the locking face 711

clears the inner edge 309 and snaps into engagement with the inner face 308 of the end section 307.

5 The other radiating section 402 is then snapped into the opposite socket 702 in a similar manner. With the clip in place as shown in Figure 7C, the longitudinal rib 707 maintains a precise spacing between the radiating sections 301,402.

10 Figure 8 shows a single dual polarization folded dipole antenna module 800 according to a second embodiment of the present invention. The ground plane and dielectric spacers are not shown. The antenna module 800 is identical to the module 500 shown in Figure 5, except it is provided as a single self-contained module with inputs 840 and 841.

15 In a variable downtilt antenna (not shown), a number of single modules 800 can be arranged in a line and ganged together with cables, circuit-board splitters, and variable differential phase shifters for adjusting the phase between the modules. For instance, the differential phase shifters described in US2002/0126059A1 and US2002/0135524A1 may be used.

20 The transition coupling the coaxial transmission line 360 with the RF input section 340 is shown in Figures 9-13. The coaxial transmission line 360 has a central conductor 361 and a cylindrical coaxial conductive sheath 362 separated from the central conductor by a dielectric 363. An insulating jacket 364 encloses the sheath 362.

25

A metal ground transition body 370 has a cylindrical bore 371 which receives the sheath 362. The sheath 362 is soldered into the bore 371 by placing the cable into the bore, heating the joint and injecting solder through a hole 373 in the body 370 and into a gap 374 between the end of the body 370 and the jacket 364. The
30 outer body 370 has an outer flange formed with a chamfered surface 372.

A metal transition ring 375 has a bore which receives the ground transition body 370. The bore has a chamfered surface 376 which engages the chamfered surface 372 of the body 370.

5

A plastic insulating washer 377 is provided between the transition ring 375 and the ground plane 101. The ground plane 101, washer 377 and transition ring 375 are provided with three holes which each receive an externally threaded shaft of a respective bolt 378.

10

The central conductor 361 extends beyond the end of the sheath, and is received in a bore of a plastic insulating collar 380. The collar 380 has a body portion received in a hole in the ground plane 101, and an outwardly extending flange 381 which engages an inwardly extending flange 382 of the ground transition body 370.

15

The three holes in the transition ring 375 are internally threaded so that when the bolts 378 are tightened, the chamfered surface 376 of the transition ring engages the chamfered surface 372 and forces the ground transition body 370 into conductive engagement with the ground plane 101. The chamfered surfaces 372,376 also generate a sideways centering force which accurately centers the coaxial cable.

20

It should be noted that this arrangement does not require any direct soldering between the ground transition body 370 and the ground plane 101.

25

A metal centre pin 385 is formed with a relatively wide base 386 which is hexagonal in cross-section, a relatively narrow shaft 385 which is externally threaded and circular in cross-section, and a shoulder 389. The base 386 has a cup which receives the central conductor 361, which is soldered in place. Soldering

30

is performed by first placing a bead of solder in the cup, then inserting the conductor 361, heating the joint and injecting solder through a hole 390 in the base 386. The shaft 385 passes through a hole in the RF input section 340, and through a metal locking washer 387 and hexagonal nut 388.

5

When the nut 388 is tightened, the shoulder 389 is forced into conductive engagement with the RF input section 340. The parts are precisely machined so as to provide a desired spacing between the ground plane 101 and RF input section 340.

10

It should be noted that this arrangement does not require any direct soldering between the ground centre pin 385 and the RF input section 340.

15

The transition employs a mechanical joint between the ground plane 101 and the transition body 370, and between the centre pin base 386 and the RF input section. These mechanical joints are more repeatable than the solder joints shown in the prior art. The pressure of the mechanical joints can be accurately controlled by using a torque wrench to tighten the nut 388 and bolts 378. The ground plane 101 and RF input section 340 can be formed from a metal such as Aluminium, which cannot form a solder joint.

20

An alternative dipole box configuration is shown in Figure 14. In contrast to the "ring" structure shown in figures 1,5 and 8, the radiating sections 301',302',401',402' are formed in a generally "square" structure. In common with the "ring" structure, the radiating sections are arranged in a "box" configuration around a central region. In a further alternative configuration (not shown) the four dipoles may be arranged in a "cross" configuration with the radiating sections extending radially from a central point.

25

The antennas shown in the figures are designed for use in the "cellular" frequency band: that is 806-960 MHz. Alternatively the same design (typically the cabled together version with a PCB power splitter) may operate at 380-470 MHz. Another possible band is 1710-2170 MHz. However, it will be appreciated that the invention could be equally applicable in a number of other frequency bands.

The preferred field of the invention is shown in Figure 15. The antennas are typically incorporated in a mobile wireless communications cellular network including base stations 900. The base stations include masts 901, and antennas 902 mounted on the masts 901 which transmit and receive downlink and uplink signals to/from mobile devices 903 currently registered in a "cell" adjacent to the base station.

While the invention is susceptible to various modifications and alternative forms, specific embodiments have been shown by way of example in the drawings and have been described in detail herein. However, it should be understood that the invention is not intended to be limited to the particular forms disclosed. Rather, the invention is to cover all modifications, equivalents, and alternatives falling within the spirit and scope of the invention as defined by the appended claims

CLAIMS

1. A dual polarized folded dipole antenna comprising:
- 5 a first unit configured for transmitting and/or receiving signals in a first polarization direction; and
- a second unit configured for transmitting and/or receiving signals in a second polarization direction different to the first polarization direction,
- 10 wherein each unit includes a conductor having a feed section, a radiator input section, and at least one radiating section integrally formed with the radiator input section and the feed section, the radiating section including first and second ends, a fed dipole and a passive dipole, the fed dipole being connected to the radiator input section, the passive dipole being disposed in spaced relation to the fed dipole to form a gap, the passive dipole being shorted to the fed dipole at the first and second ends.
- 15
2. A dual polarized folded dipole antenna according to claim 1 wherein the feed section is a microstrip feed section having an adjacent ground plane on one side only.
- 20
3. A dual polarized folded dipole antenna according to claim 1 further comprising a ground plane, wherein the feed section is an air suspended feed section separated from the ground plane by an air gap.
- 25
4. A dual polarized folded dipole antenna according to claim 1 wherein the antenna comprises a slant polarized antenna with two or more modules arranged along an antenna axis, wherein the first and second polarization directions are at an angle to the antenna axis.
- 30

5. A dual polarized folded dipole antenna according to claim 1 wherein the first unit includes a first pair of folded dipoles, the second unit includes a second pair of folded dipoles, each folded dipole including a respective radiator input section and a respective radiating section, and wherein the two pairs of radiating sections are arranged in a box configuration around a central region.
6. A dual polarized folded dipole antenna according to claim 5 wherein the box configuration is a ring configuration.
7. A dual polarized folded dipole antenna according to claim 5 wherein the box configuration is a square configuration.
8. A dual polarized folded dipole antenna according to claim 1 further comprising a ground plane, wherein the radiating sections extend substantially parallel with the ground plane.
9. A dual polarized folded dipole antenna according to claim 1 further comprising a ground plane, wherein the radiator input section includes a pair of feed legs which each extend substantially transversely to the ground plane.
10. A dual polarized folded dipole antenna according to claim 1 wherein the radiator input section includes a balun transformer.
11. A dual polarized folded dipole antenna according to claim 1 wherein the radiator input section includes a splitter, first and second feedlines which meet said feed section at said splitter so as to complete a closed loop including the first and second feedlines and the radiating section, and a phase delay element for introducing a phase difference between the first and second feedlines.

12. A folded dipole antenna comprising:

a ground plane

5

a conductor having a feed section extending adjacent the ground plane and spaced therefrom by a dielectric, a radiator input section, and at least one radiating section integrally formed with the radiator input section and the feed section, the radiating section including first and second ends, a fed dipole and a passive dipole, the fed dipole being connected to the radiator input section, the passive dipole being disposed in spaced relation to the fed dipole to form a gap, the passive dipole being shorted to the fed dipole at the first and second ends,

10

wherein the feed section is a microstrip feed section having an adjacent ground plane on one side only, and

wherein the radiator input section includes a balun transformer.

15

13. A folded dipole antenna according to claim 12 wherein the feed section is an air suspended feed section separated from the ground plane by an air gap.

20

14. A folded dipole antenna comprising:

a ground plane

25

a conductor having a feed section extending adjacent the ground plane and spaced therefrom by a dielectric, a radiator input section, and at least one radiating section integrally formed with the radiator input section and the feed section, the radiating section including first and second ends, a fed dipole and a passive dipole, the fed dipole being connected to the radiator input section, the passive dipole being disposed in spaced relation to the fed dipole to form a gap, the passive dipole being shorted to the fed dipole at the first and second ends,

wherein the feed section is a microstrip feed section having an adjacent ground plane on one side only, and

wherein the radiator input section includes a splitter, first and second feedlines which meet said feed section at said splitter so as to complete a closed loop including the first and second feedlines and the radiating section, and a phase delay element for introducing a phase difference between the first and second feedlines.

5

10

15. A folded dipole antenna according to claim 14 wherein the feed section is an air suspended feed section separated from the ground plane by an air gap.

15

20

25

16. A coaxial to microstrip transition comprising:
- a ground plane;
 - a microstrip transmission line on a first side of the ground plane;
 - a coaxial transmission line on a second side of the ground plane opposite to the first side of the ground plane, the coaxial transmission line having a central conductor coupled to the microstrip line, a coaxial cylindrical conductor sleeve coupled to the ground plane, and a dielectric material between the central conductor and the sleeve,
 - a conductive ground transition body in conductive engagement with the sleeve; and
 - a ground locking member applying a force to the ground transition body so as to force the ground transition body into conductive engagement with the ground plane.

17. A coaxial to microstrip transition according to claim 16 wherein the microstrip transition line is an air suspended transition line separated from the ground plane by an air gap.

30

18. A coaxial to microstrip transition according to claim 16 wherein the ground transition body has a cylindrical inner bore in conductive engagement with the sleeve, and an outwardly extending flange which engages the ground locking member.

5

19. A coaxial to microstrip transition according to claim 18 wherein the central conductor passes through a hole in the ground plane, and wherein the flange has a chamfered surface which engages the ground locking member and generates a centering force which centers the central conductor with respect to the hole in the ground plane.

10

20. A coaxial to microstrip transition according to claim 16 wherein the microstrip transition line is an air suspended transition line separated from the ground plane by an air gap.

15

21. A coaxial to microstrip transition comprising:

a ground plane;

a microstrip transmission line on a first side of the ground plane;

a coaxial transmission line on a second side of the ground plane opposite to the first side of the ground plane, the coaxial transmission line having a central conductor coupled to the microstrip line, a coaxial cylindrical conductor sleeve coupled to the ground plane, and a dielectric material between the central conductor and the sleeve,

20

a conductive line transition body in conductive engagement with the central conductor; and

25

a line locking member applying a force to the line transition body so as to force the line transition body into conductive engagement with the microstrip line.

- 5 22. A coaxial to microstrip transition according to claim 21 wherein the line transition body has a relatively narrow shaft passing through a hole in the microstrip transmission line, a relatively wide base, and a shoulder between the relatively narrow shaft and the relatively wide base, the shoulder being forced into conductive engagement with the microstrip line.
- 10 23. A coaxial to microstrip transition according to claim 21 wherein the line transition body has a cylindrical inner bore in conductive engagement with the central conductor.
- 15 24. A coaxial to microstrip transition according to claim 21 wherein the line transition body has an externally threaded shaft which passes through a hole in the microstrip transmission line, and the line locking member has an internally threaded bore which engages the externally threaded shaft.
- 20 25. A coaxial to microstrip transition according to claim 21 wherein the microstrip transition line is an air suspended transition line separated from the ground plane by an air gap.
- 25 26. A method of constructing a coaxial to microstrip transition, the method comprising:
arranging a microstrip transmission line on a first side of a ground plane;
arranging a coaxial transmission line on a second side of the ground plane opposite to the first side of the ground plane, the coaxial transmission line having a central conductor coupled to the microstrip line, a coaxial cylindrical conductor sleeve coupled to the ground plane, and a dielectric material between the central conductor and the sleeve,

arranging a conductive ground transition body in conductive engagement with the sleeve; and

applying a force to the ground transition body so as to force the ground transition body into conductive engagement with the ground plane.

5

27. A method of constructing a coaxial to microstrip transition, the method comprising:

arranging a microstrip transmission line on a first side of a ground plane;

10

arranging a coaxial transmission line on a second side of the ground plane opposite to the first side of the ground plane, the coaxial transmission line having a central conductor coupled to the microstrip line, a coaxial cylindrical conductor sleeve coupled to the ground plane, and a dielectric material between the central conductor and the sleeve,

15

arranging a conductive line transition body in conductive engagement with the central conductor; and

20

applying a force to the line transition body so as to force the line transition body into conductive engagement with the microstrip line.

28. An electrically insulating retaining element for retaining together adjacent ends of a pair of dipoles, the element comprising a body portion having a pair of sockets on opposite side of the body portion; and a pair of resilient members which each obstruct a respective socket and resiliently flex, when in use, to admit an end of a dipole into the socket.

25

29. An electrically insulating retaining element according to claim 28 wherein the resilient members comprise arms which extend outwardly from a

proximal end attached to the body portion to a distal end which is formed with an inwardly directed shoulder.

- 5 30. An electrically insulating retaining element according to claim 28, wherein the sockets are configured to receive an end of a dipole as a snap fit.
- 10 31. A dipole assembly comprising two or more dipoles having adjacent ends retained together by electrically insulating retaining elements, each element comprising a body portion having a pair of sockets on opposite side of the body portion; and a pair of resilient members which each obstruct a respective socket and resiliently flex, when in use, to admit an end of a dipole into the socket.
- 15 32. An assembly according to claim 31 wherein the resilient members comprise arms which extend outwardly from a proximal end attached to the body portion to a distal end which is formed with an inwardly directed shoulder.
- 20 33. An assembly according to claim 31, wherein the dipole ends are received in the sockets as a snap fit.
34. An assembly according to claim 31 wherein the dipoles are arranged end to end so as to enclose a central region.
- 25 35. An assembly according to claim 31 wherein the dipoles are folded dipoles, and wherein the adjacent ends have proximal inner edges which are engaged by the resilient member(s) to secure the dipoles in place.
36. A wireless mobile base station including an antenna according to claim 1.
- 30

37. A wireless mobile base station including an antenna according to claim 12.
- 5 38. A wireless mobile base station including an antenna according to claim 14.
- 10 39. A wireless mobile base station including an antenna with a transition according to claim 16.
40. A wireless mobile base station including an antenna with a transition according to claim 21.
- 15 41. A wireless mobile base station including a dipole assembly according to claim 31.

ABSTRACT**FOLDED DIPOLE ANTENNA, COAXIAL TO MICROSTRIP TRANSITION, AND
RETAINING ELEMENT**

5

A dual polarized folded dipole antenna comprising: a first unit configured for transmitting and/or receiving signals in a first polarization direction; and a second unit configured for transmitting and/or receiving signals in a second polarization direction. Each unit includes an integrally formed feed section a radiator input section, and radiating section. The feed section is a microstrip feed section, and the radiator input section includes a balun transformer.

10

The antenna has a coaxial to microstrip transition comprising a microstrip transmission line on a first side of the ground plane; and a coaxial transmission line on a second side of the ground plane opposite to the first side of the ground plane. A conductive ground transition body is in conductive engagement with the sleeve of the coaxial line; and a ground locking member applies a force to the ground transition body so as to force the ground transition body into conductive engagement with the ground plane. A conductive line transition body is provided in conductive engagement with the central conductor, and a line locking member applies a force to the line transition body so as to force the line transition body into conductive engagement with the microstrip line.

15

20

Adjacent dipole ends are retained together by electrically insulating retaining elements. Each element comprises a body portion having a pair of sockets on opposite side of the body portion; and a pair of resilient members which each obstruct a respective socket and resiliently flex, when in use, to admit an end of a dipole into the socket.

25

DECLARATION AND POWER OF ATTORNEY

As a below named inventor, I hereby declare:

That my residence, post office address and citizenship are as stated below next to my name.

That I verily believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural inventors are named below) of the subject matter which is claimed and for which a patent is sought on the invention entitled:

FOLDED DIPOLE ANTENNA, COAXIAL TO MICROSTRIP TRANSITION, AND RETAINING ELEMENT

the specification of which (check one)

(X) is attached hereto.

() was filed on _____ as
Application Serial No. _____
and was amended on _____
(if applicable)

That I have reviewed and understand the contents of the above-identified specification, including the claim, as amended by any amendment referred to above.

That I acknowledge the duty to disclose information known to be material to patentability of this application in accordance with Title 37, Code of Federal Regulations, §1.56(a).

That I hereby claim foreign priority benefits under Title 35, United States Code, §119 of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate on this invention having a filing date before that of the application on which priority is claimed:

Prior Foreign Application(s)

Priority Claimed

☐ Yes ☐ No

(Number) (Country) (Day/Month/Year Filed)

☐ Yes ☐ No

(Number) (Country) (Day/Month/Year Filed)

I hereby claim the benefit under 35 U.S.C. § 119(e) of any United States provisional application(s) listed below.

(Application Number) (Filing Date)

(Application Number) (Filing Date)

That I hereby claim the benefit under Title 35, United States Code, §120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, §112, I acknowledge the duty to disclose material information as defined in Title 37, Code of Federal Regulations, §1.56(a) which occurred between the filing date of the prior application and the national or PCT international filing date of this application:

United States Application(s)

<u>(Application Serial No.)</u>	<u>(Filing Date)</u>	<u>(Status)-(Patented, pending, abandoned)</u>
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That all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issuing thereon.

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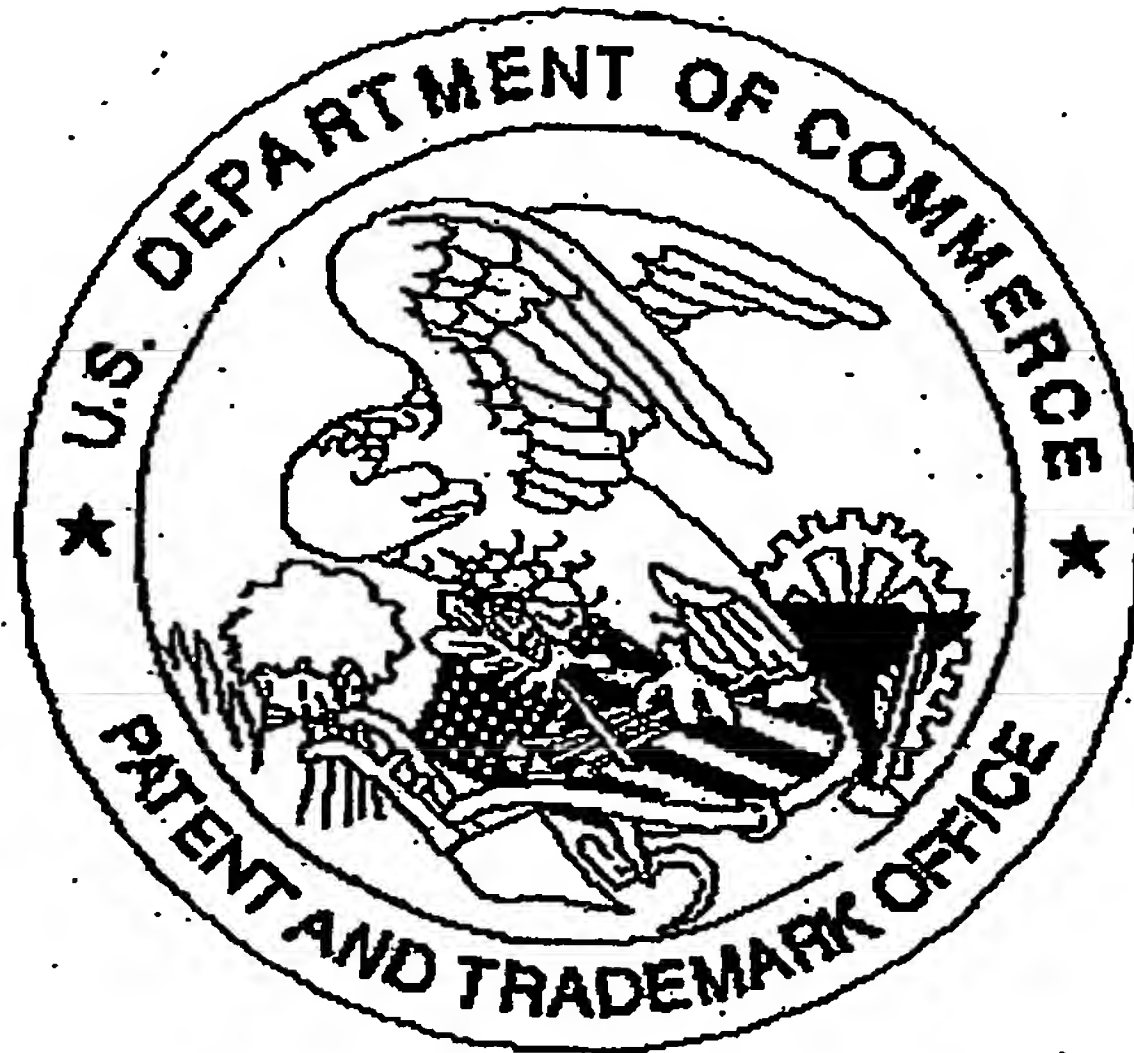
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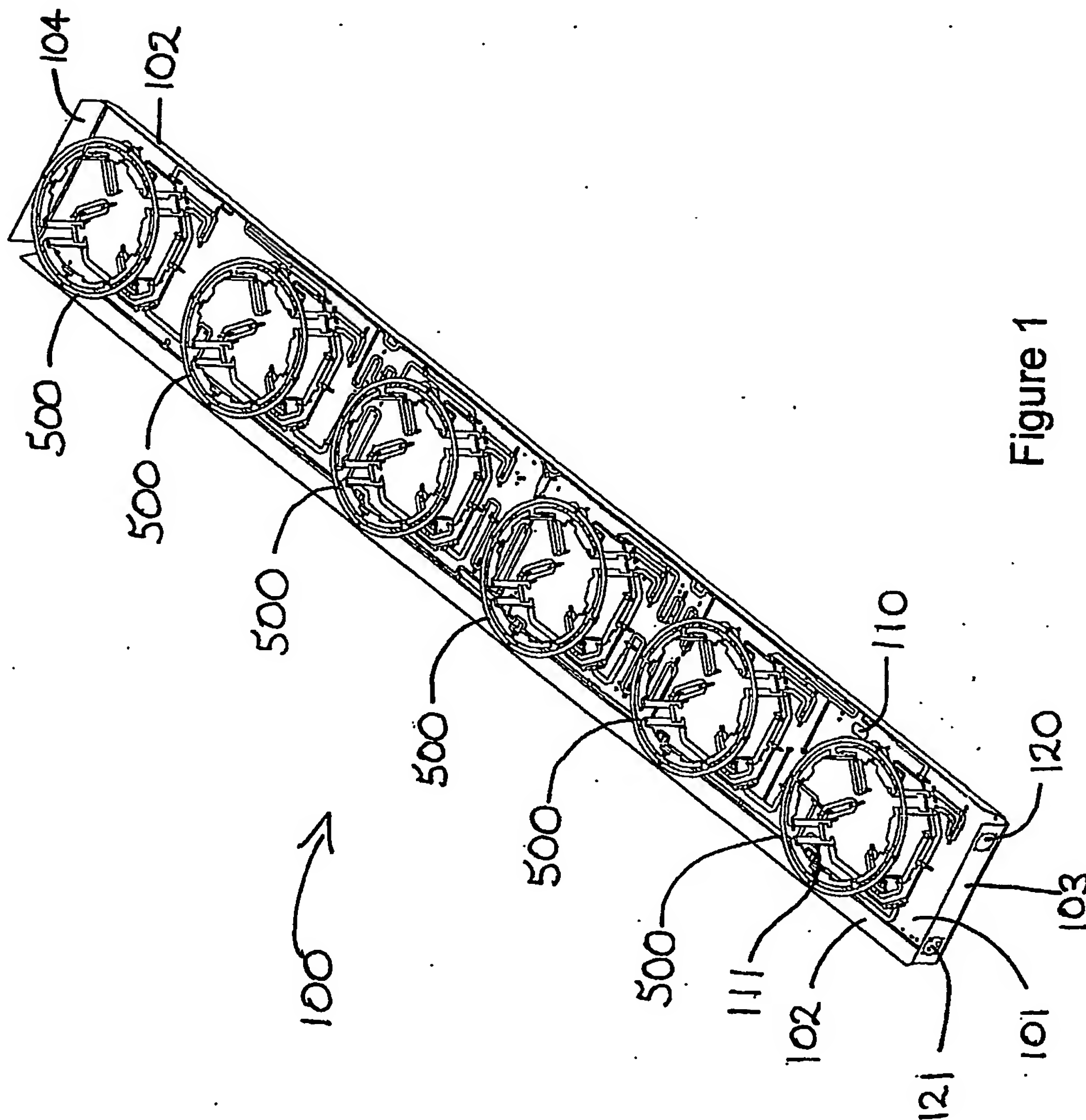


Figure 1

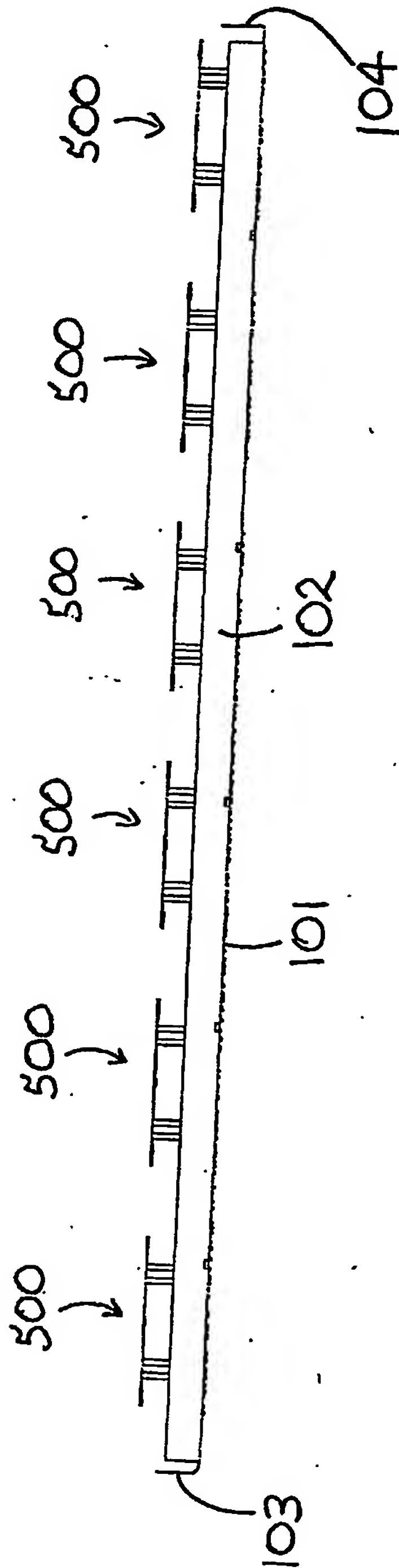


Figure 2

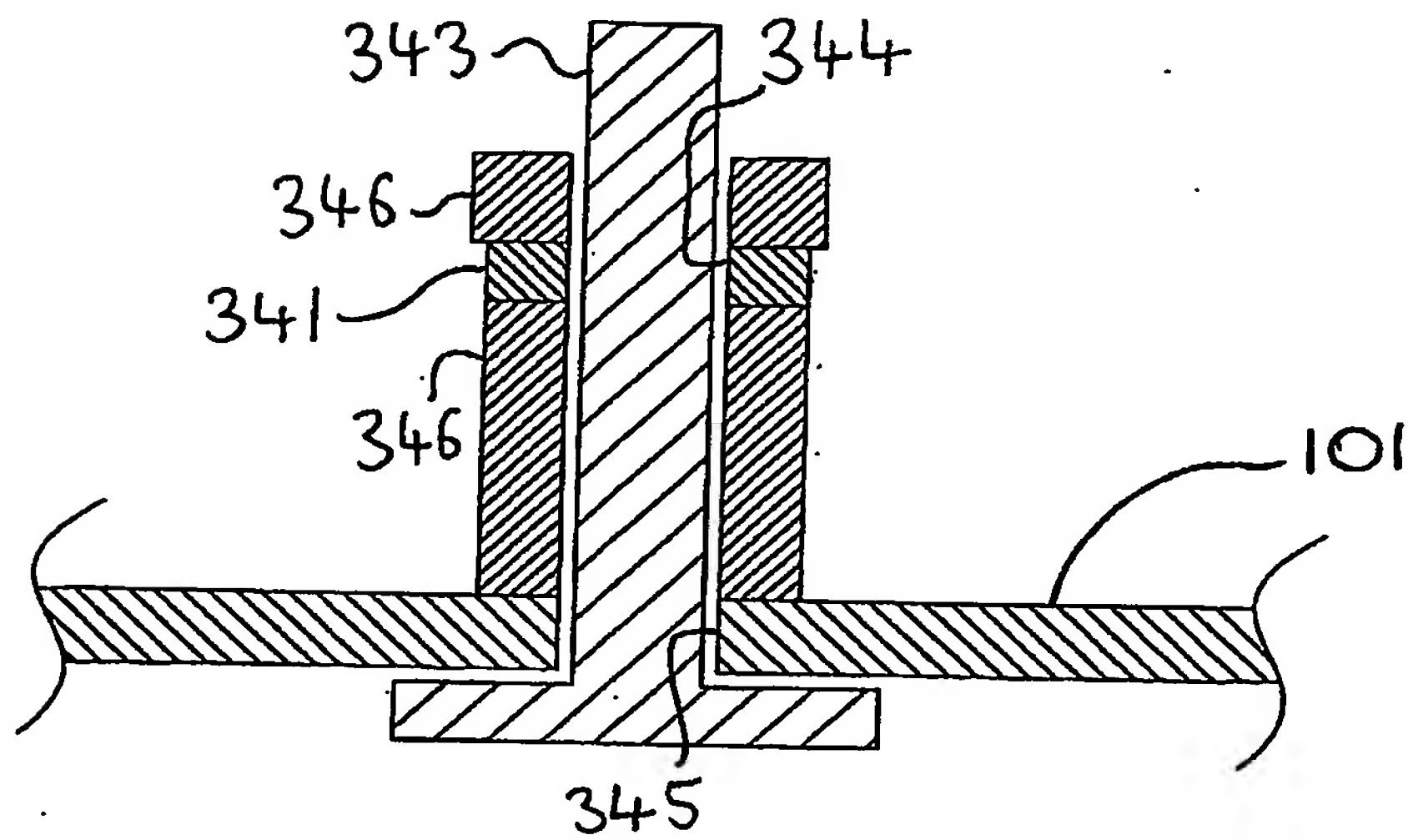


Figure 3A

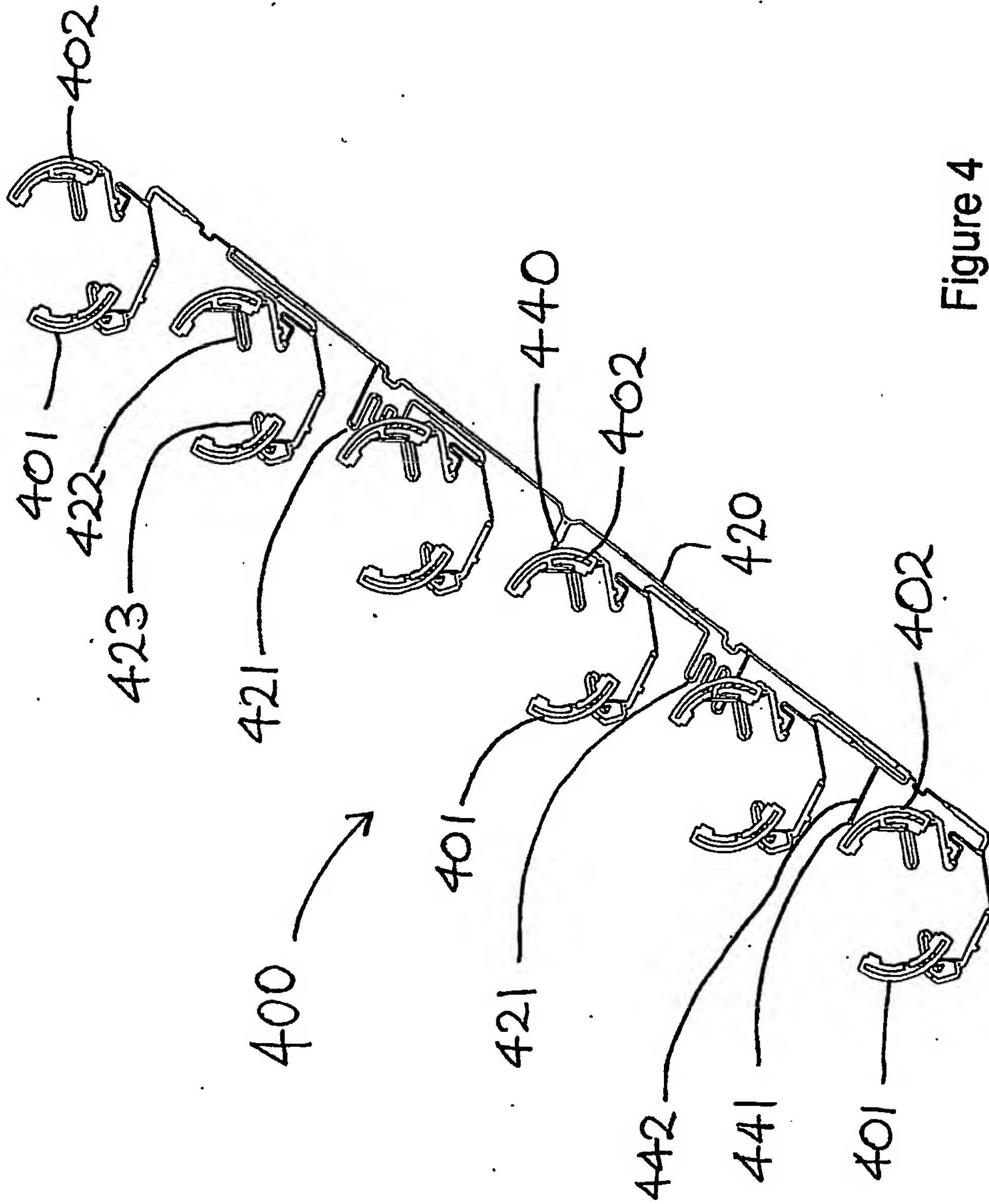


Figure 4

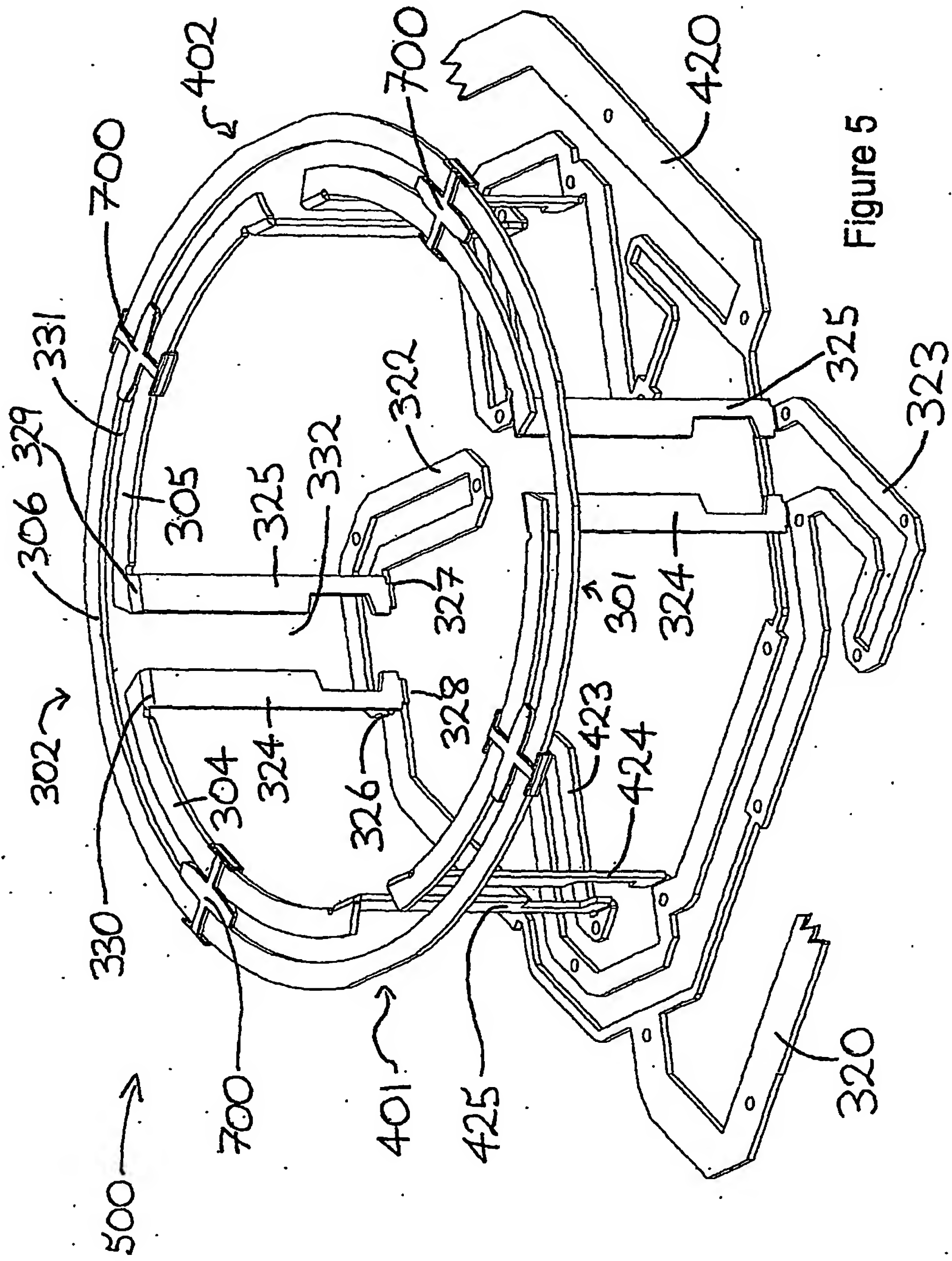


Figure 5

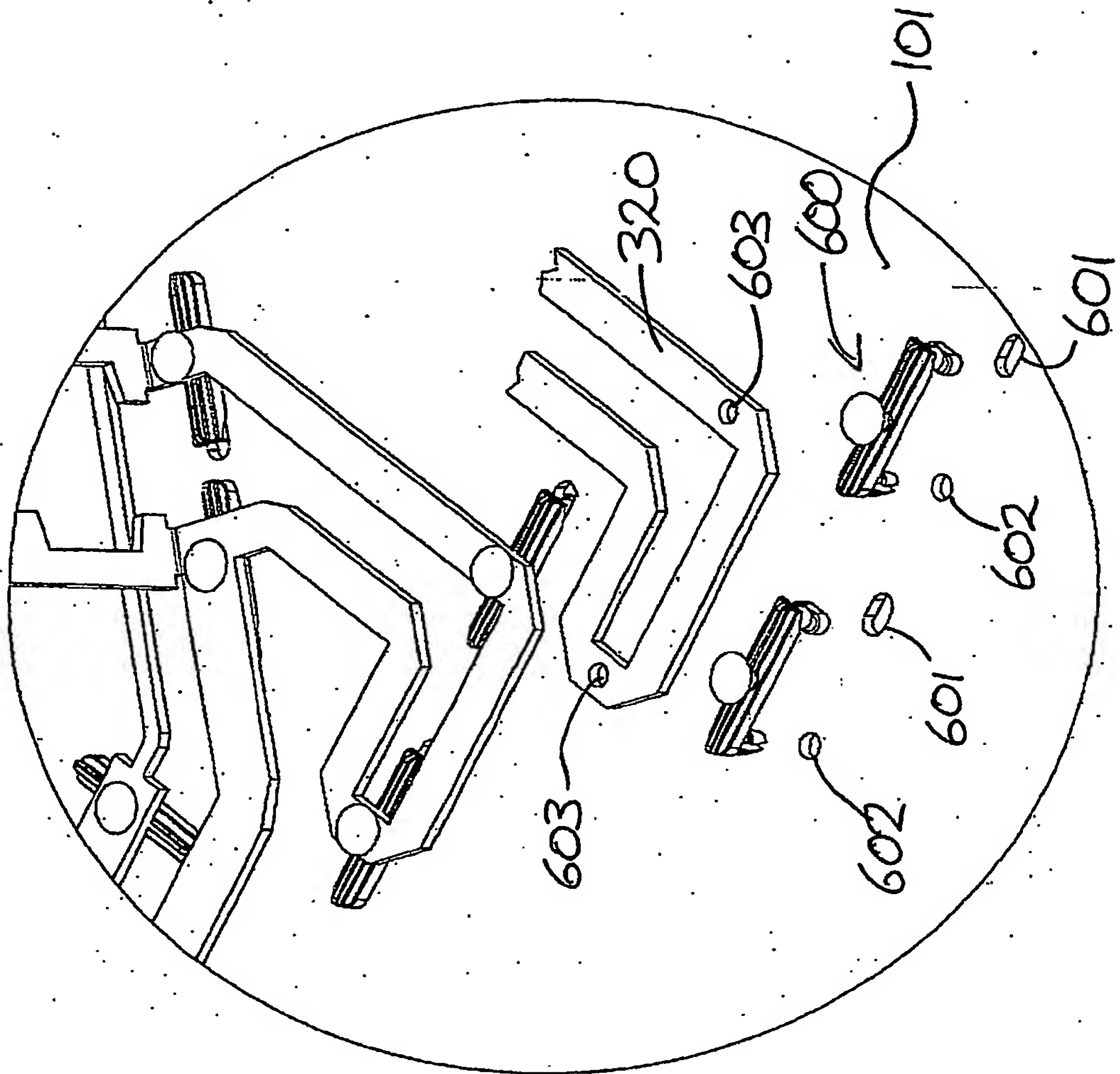


Figure 6A

Figure 6B

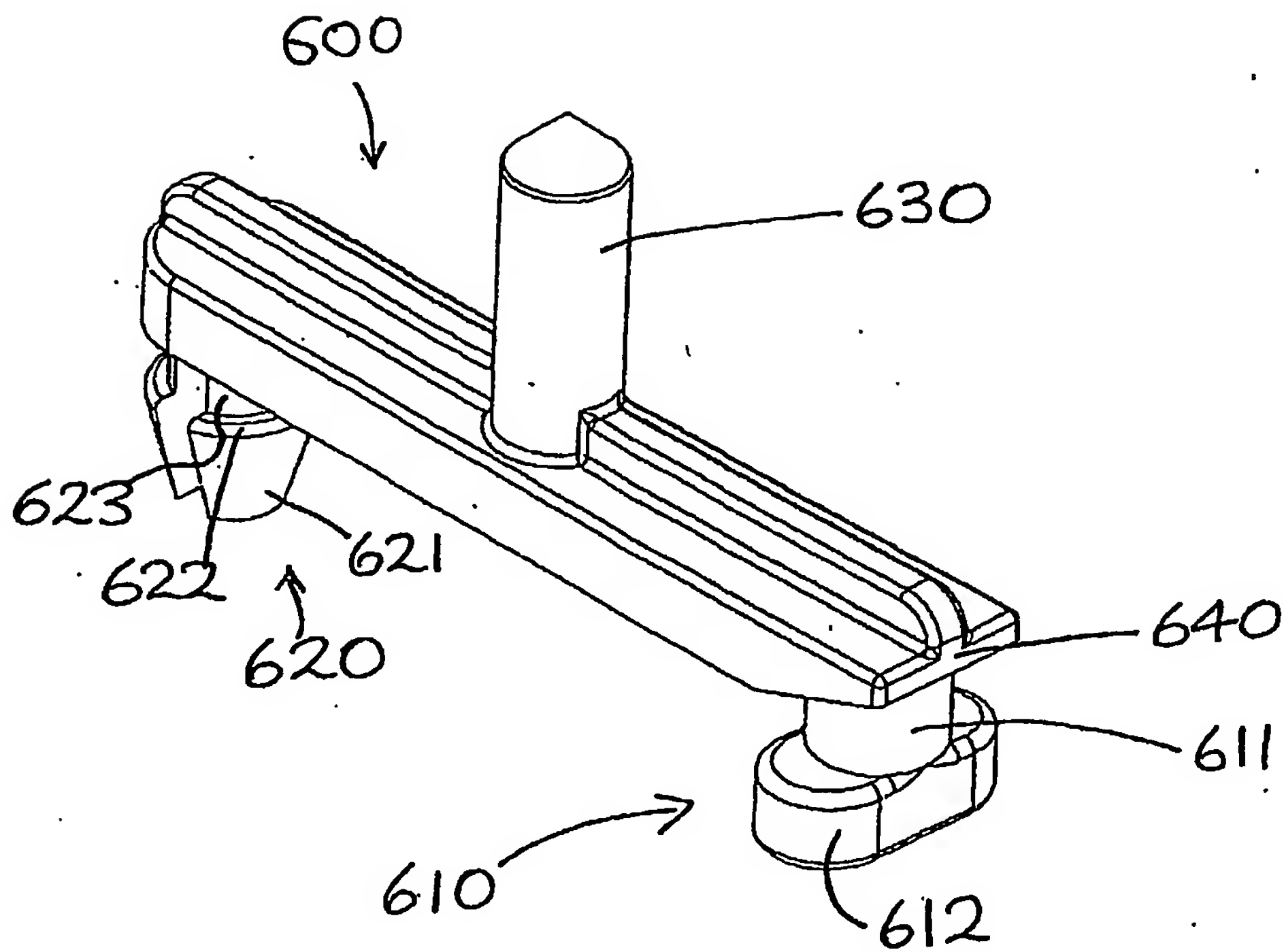


Figure 6C

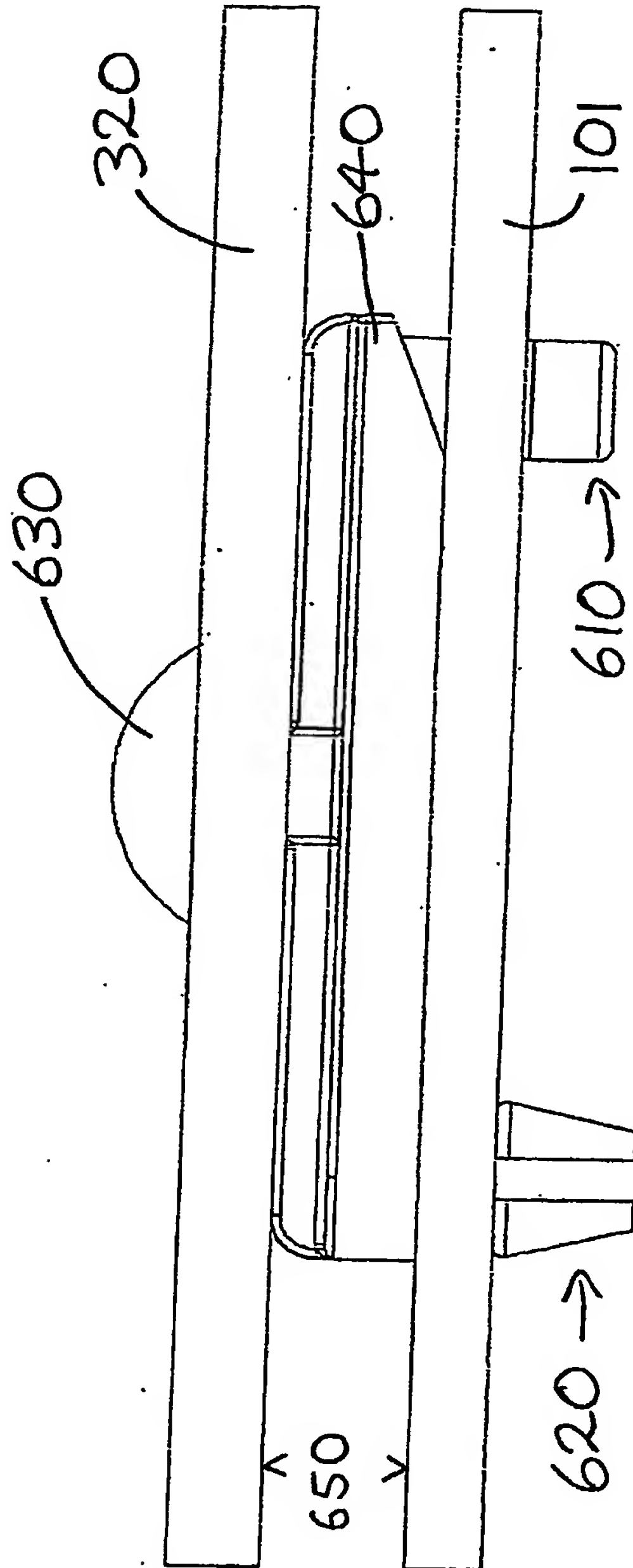
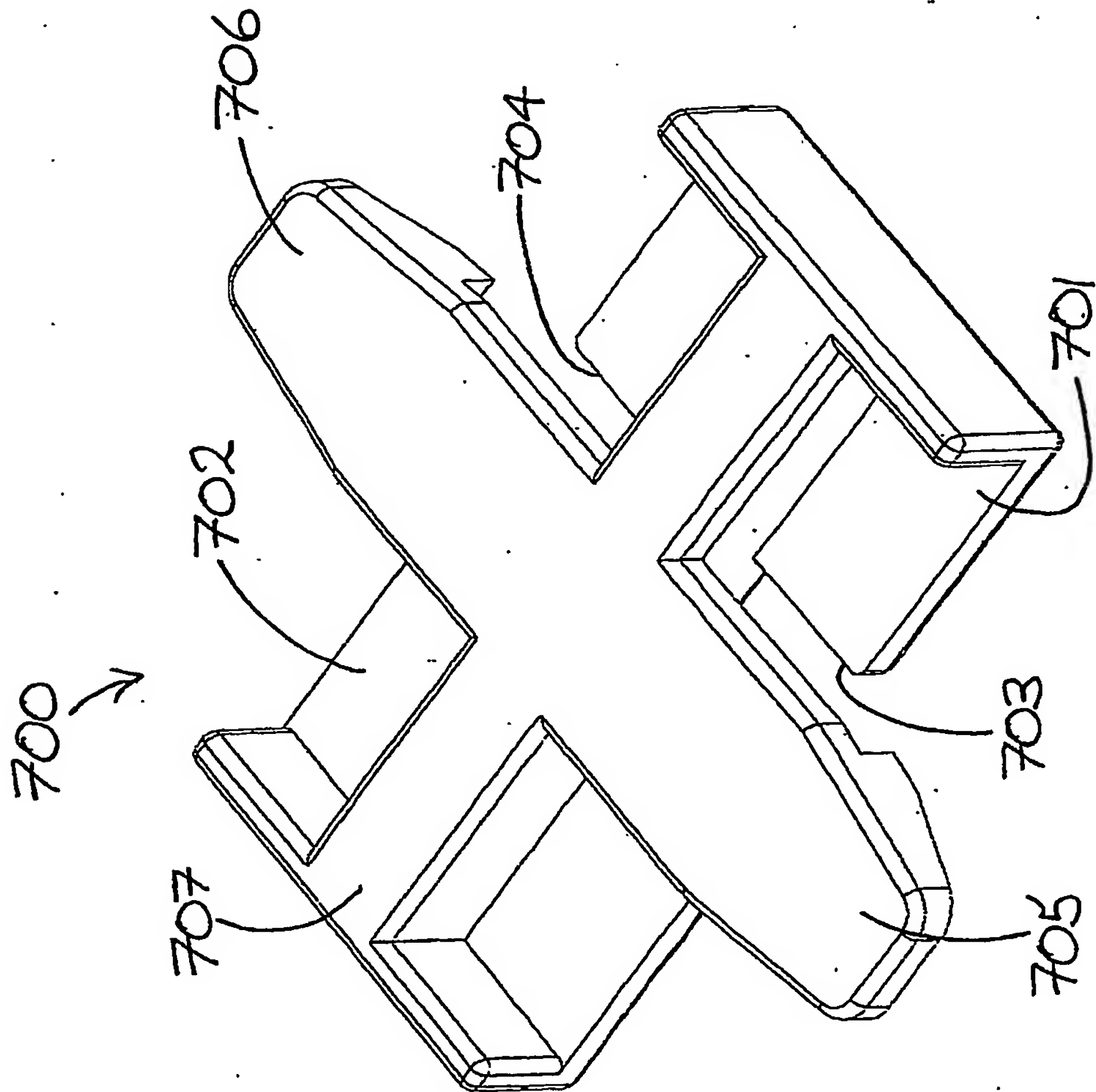


Figure 7A



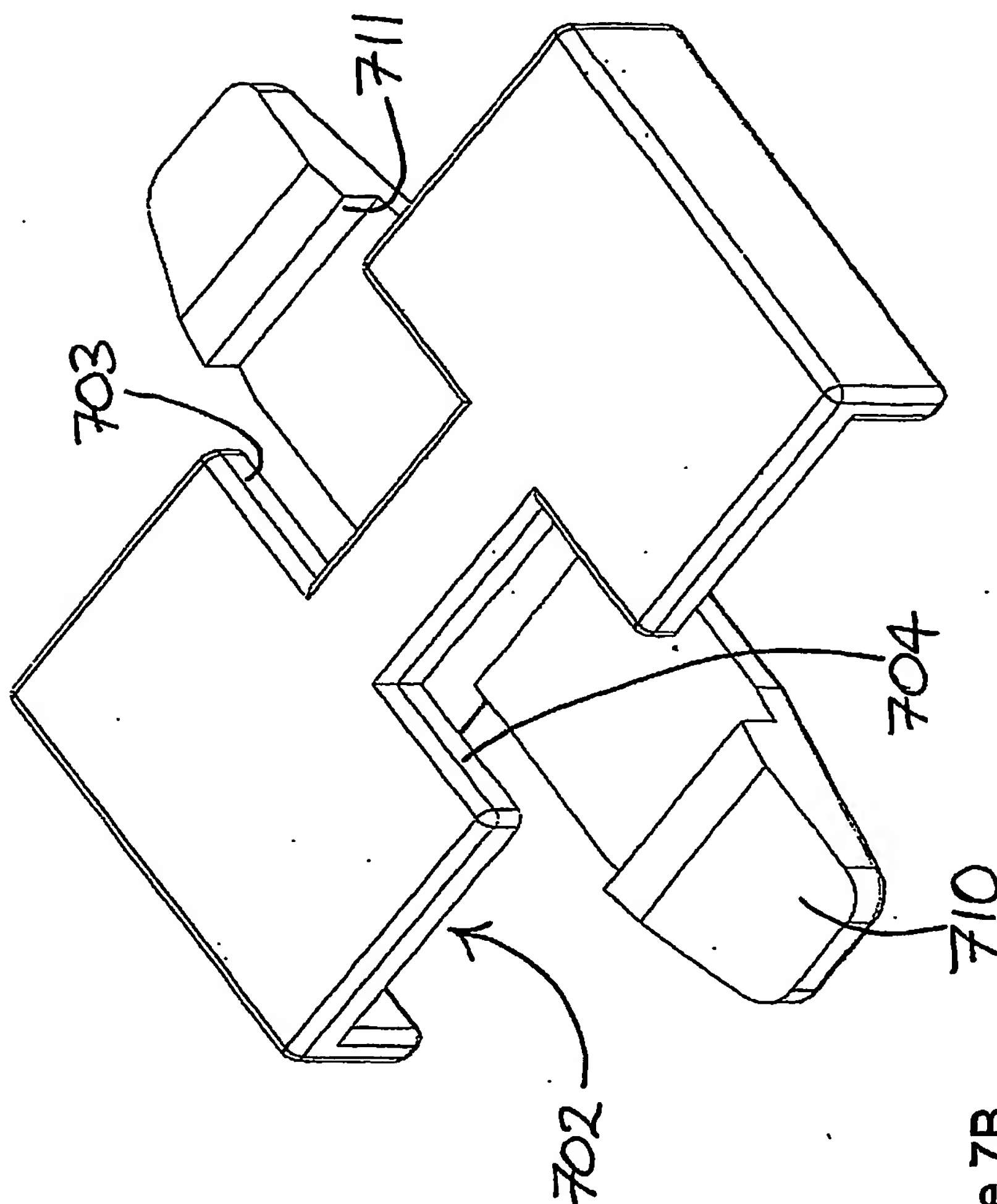


Figure 7B

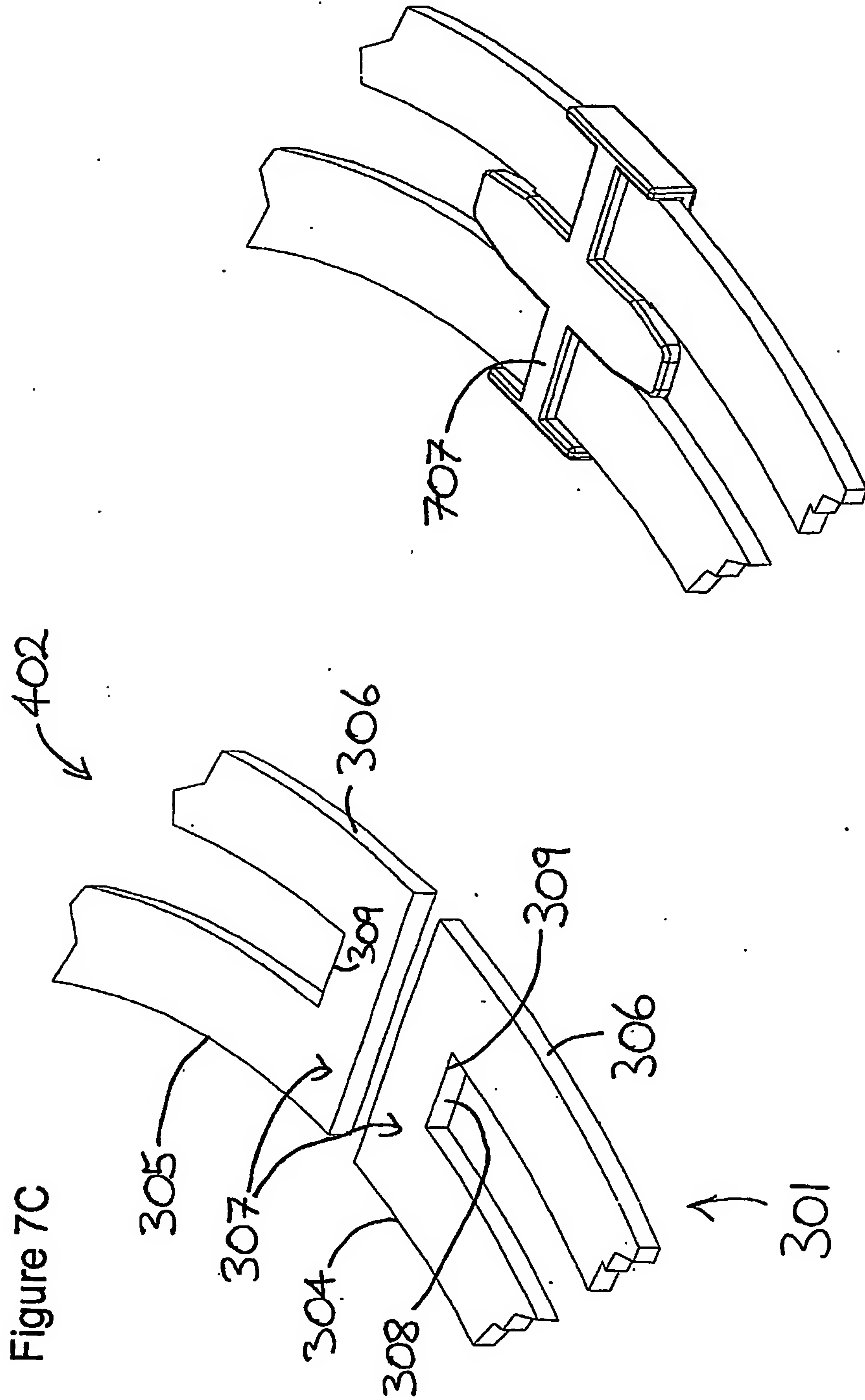
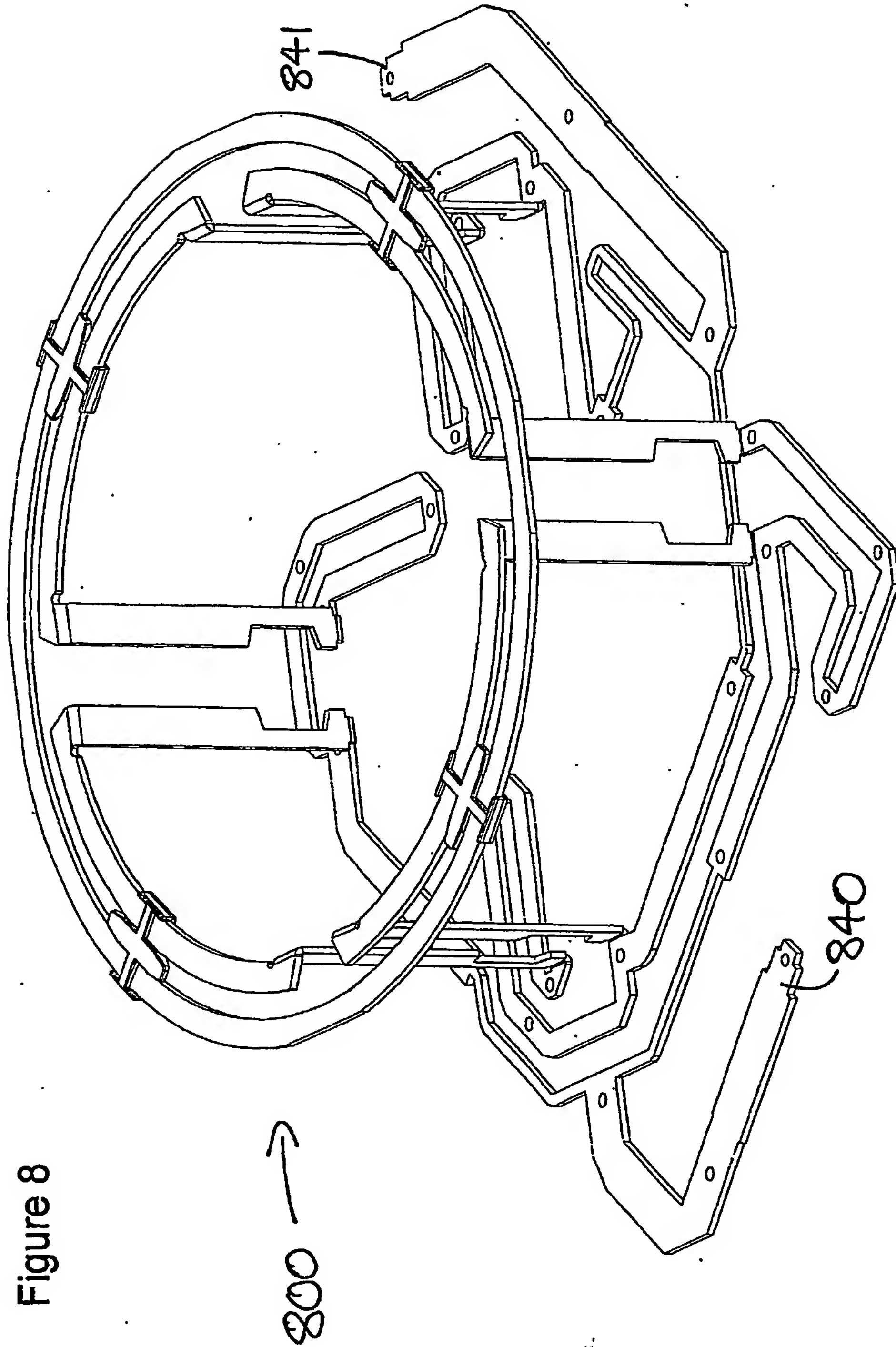


Figure 7D

Figure 7C



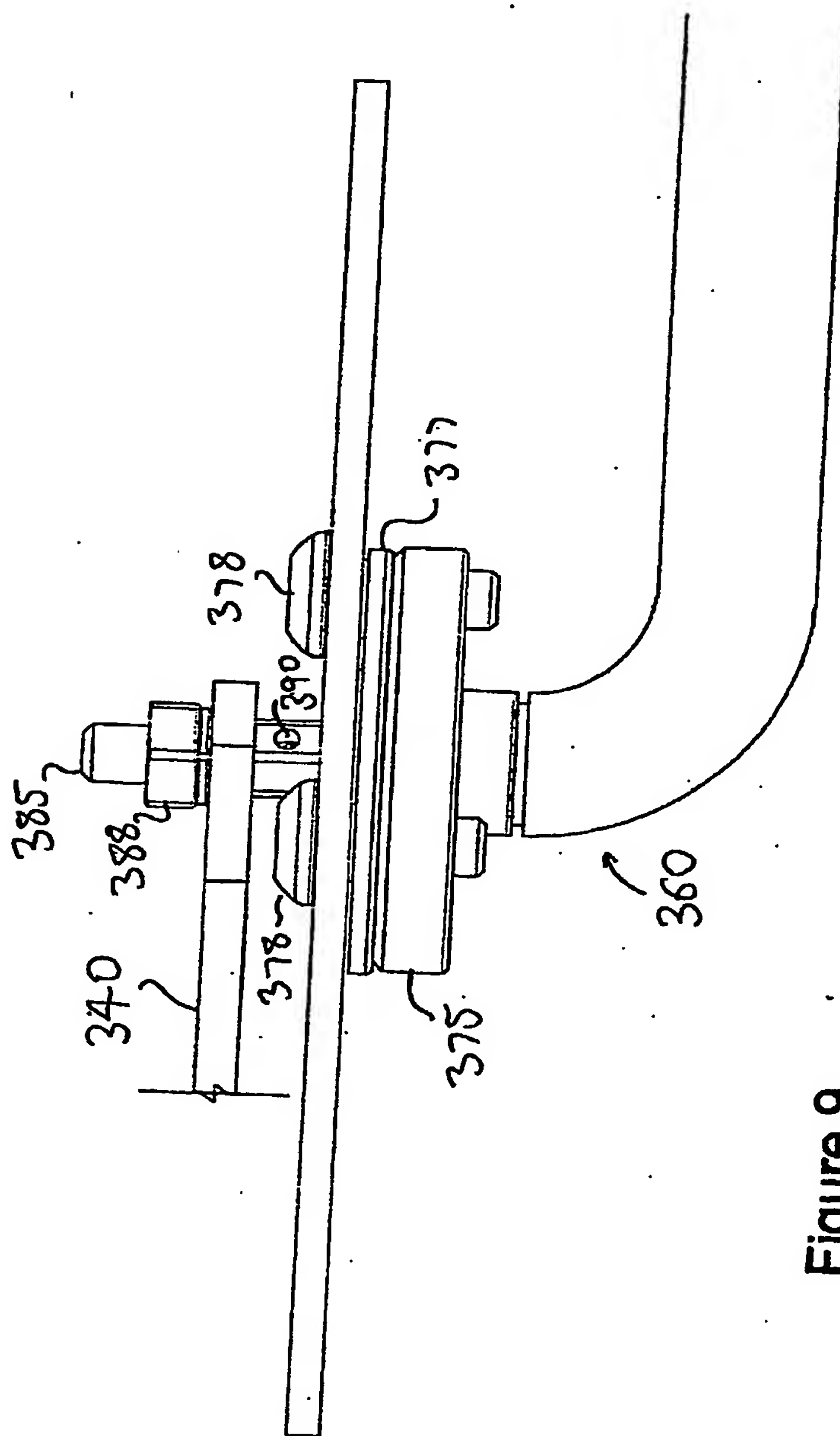


Figure 9

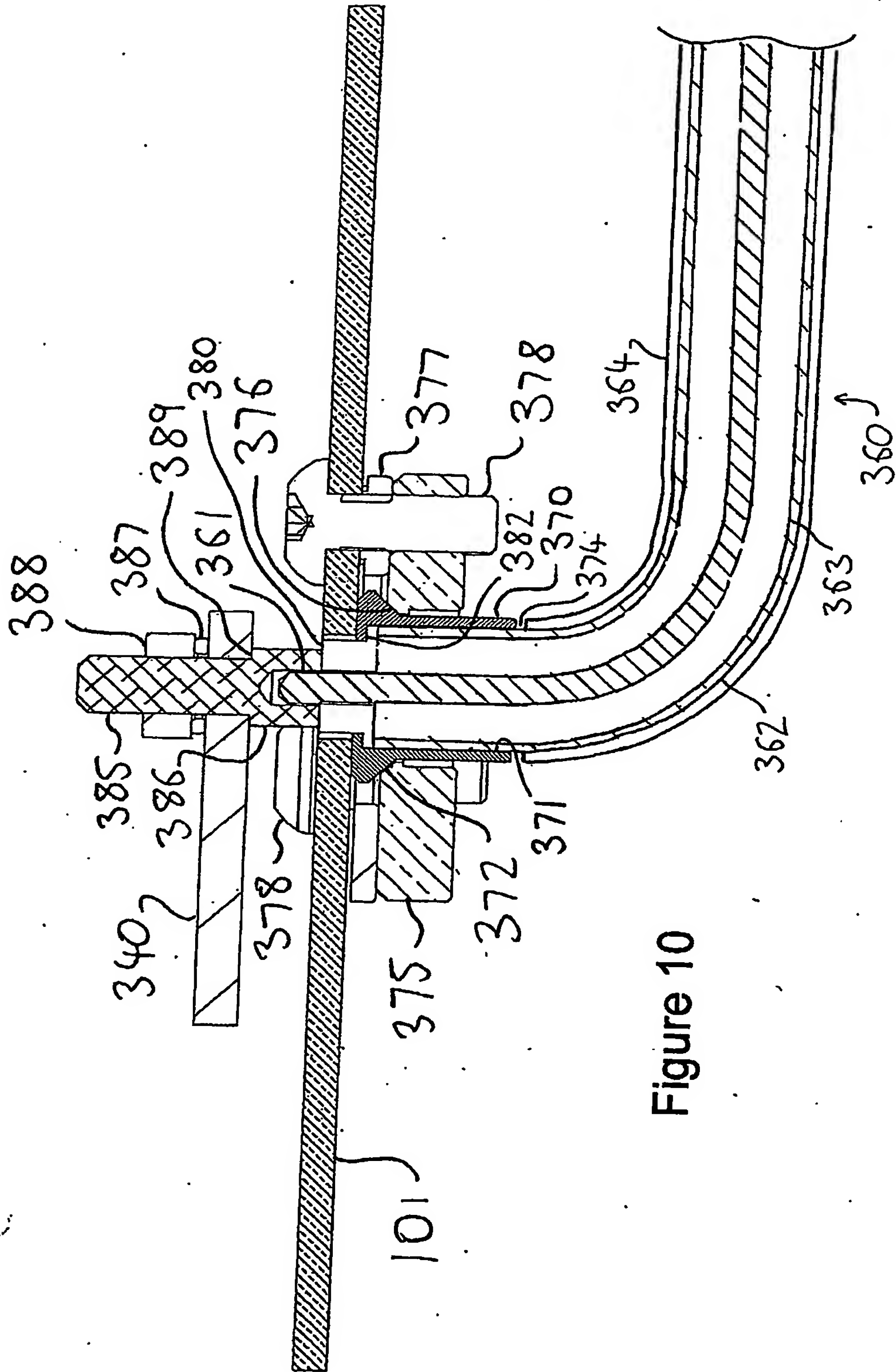


Figure 10

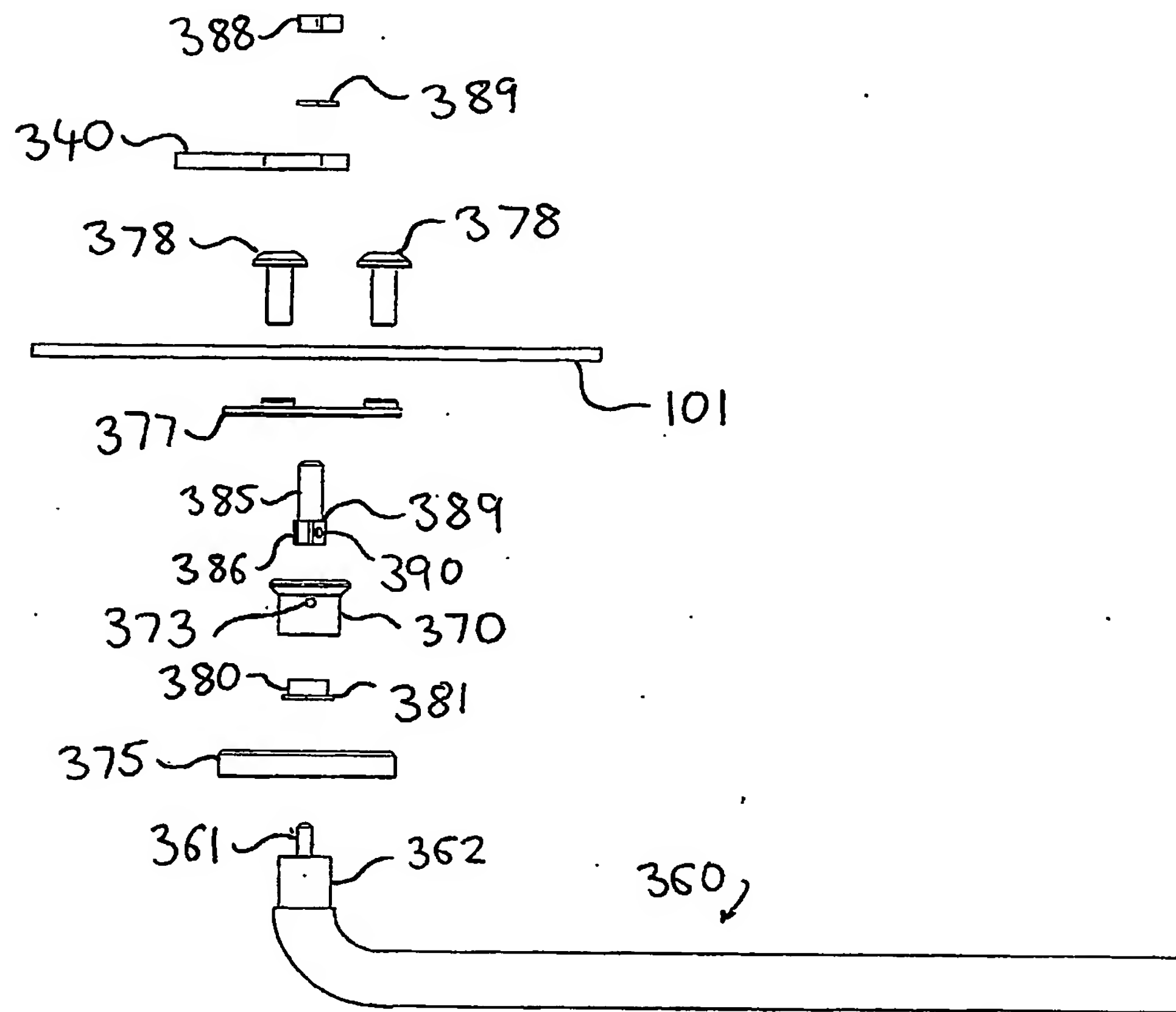


Figure 11

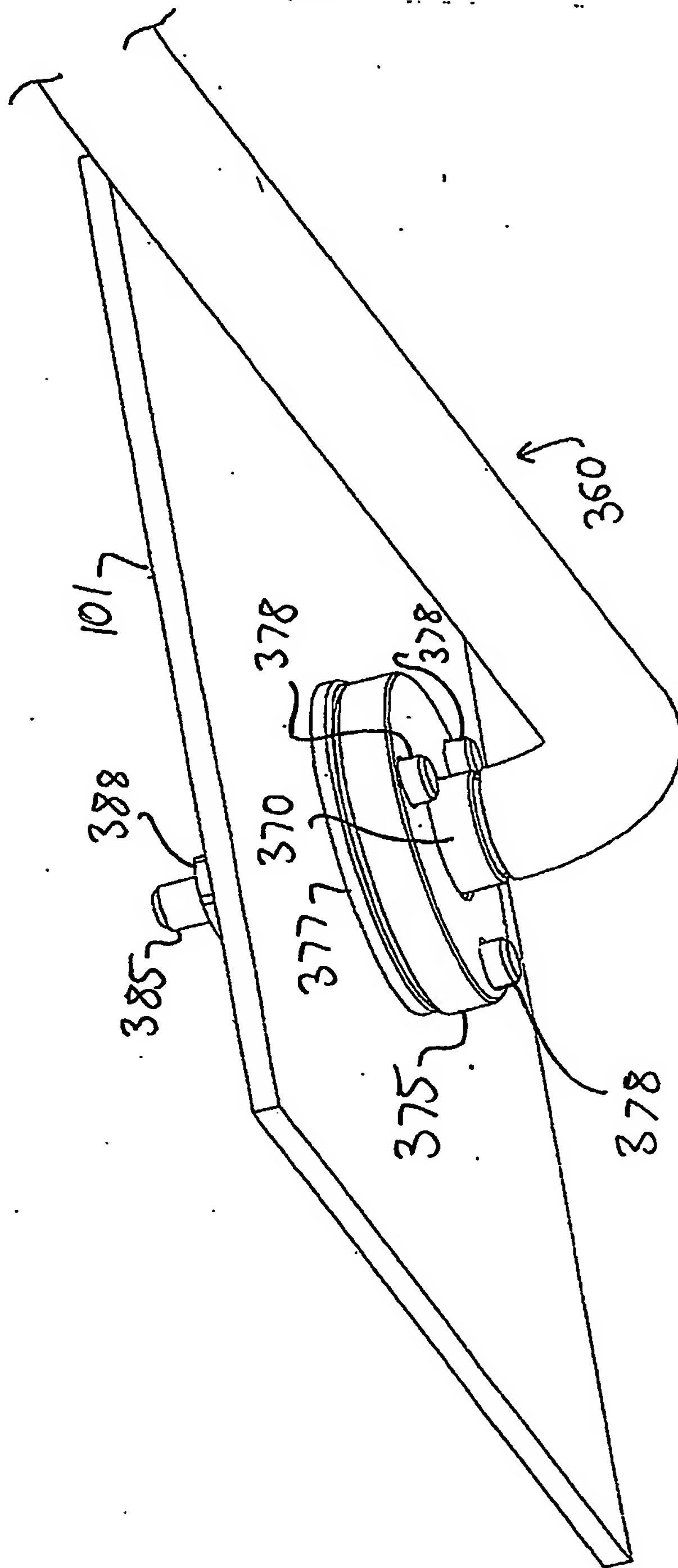
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Applicants: Bisiules et al.
Attorney Docket No. 88932

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Figure 12



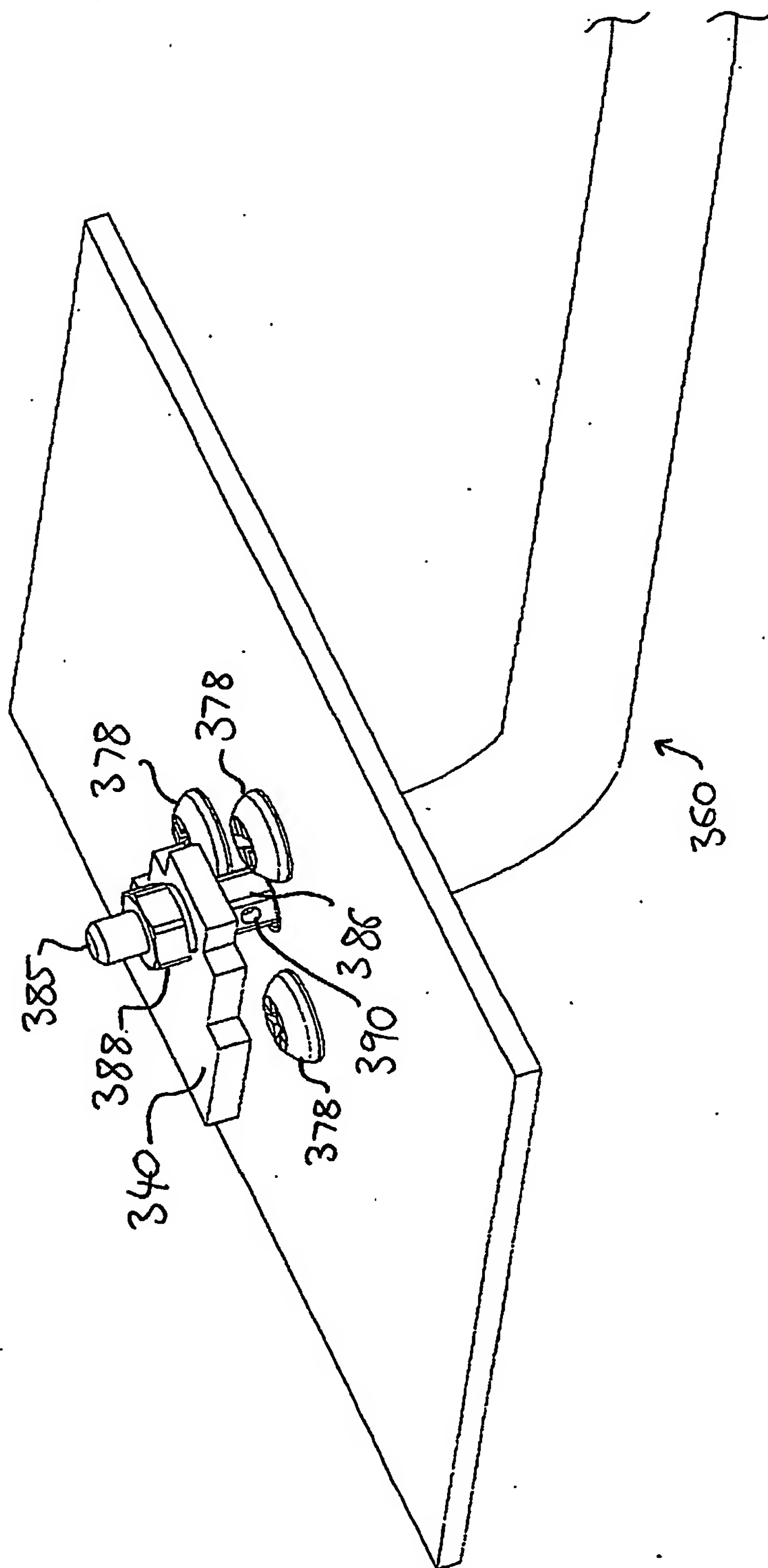


Figure 13

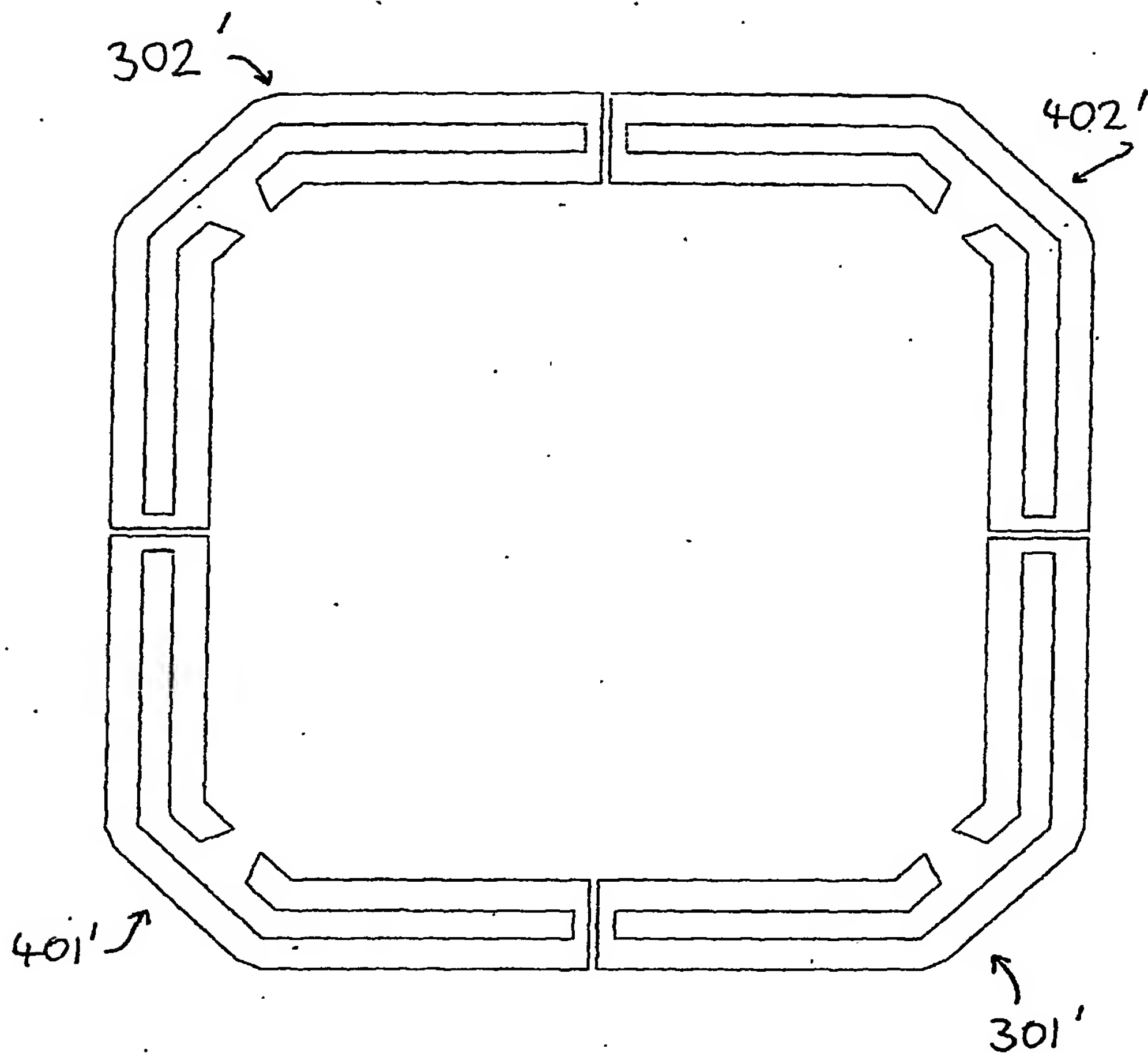
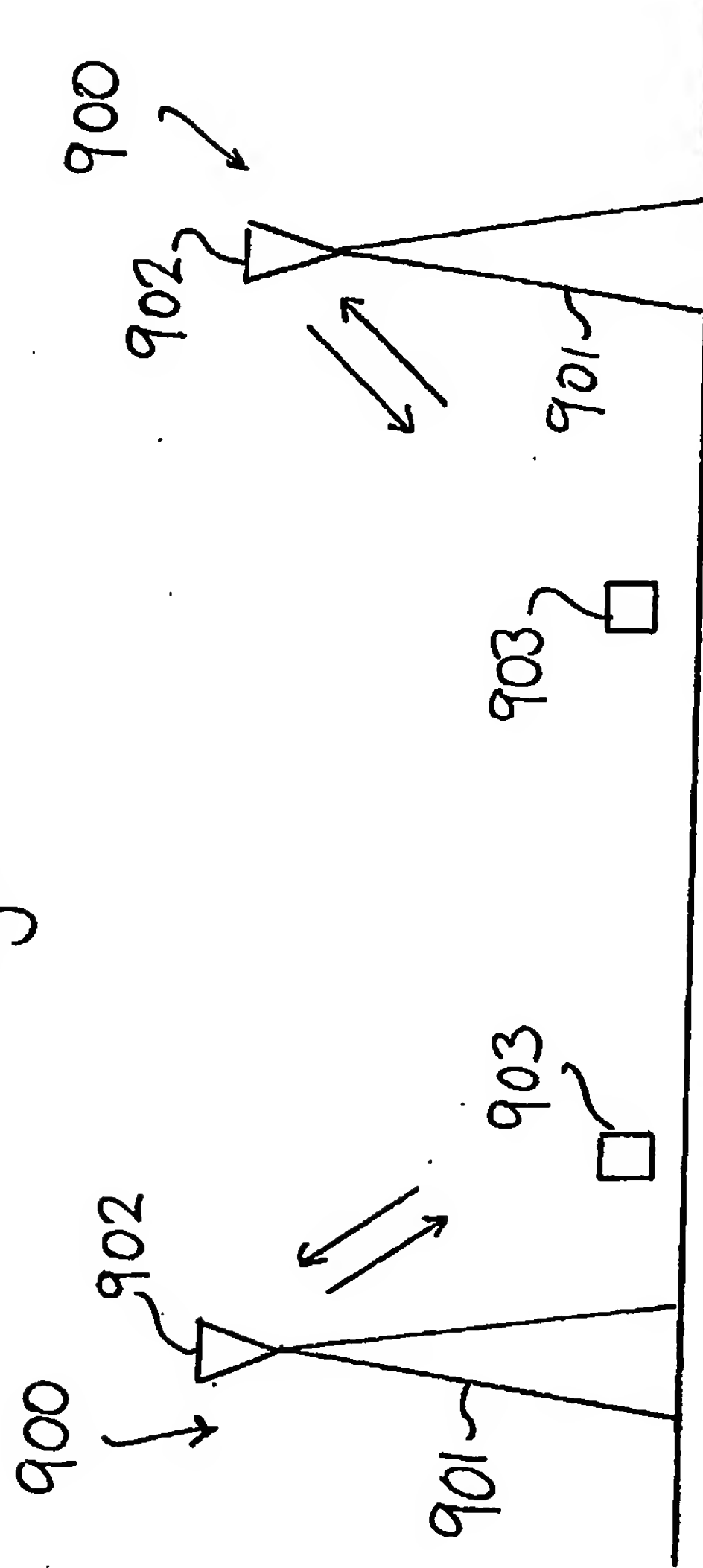


Figure 14

Figure 15



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